High sensitivity wavefront sensing with the non-linear curvature WFS

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Linearity:

The WFS response should be a linear function of the input phase

- simplifies control algorithm
- minimizes computation time -> important for fast systems

Capture range:

The WFS should be able to measure large WF errors

- the loop can be closed on natural seeing
- possible to use the WFS in open loop
- possible to "dial in" large offset aberrations

Sensitivity:

The WFS should make efficient use of the incoming photons

- the AO system can then maintain high performance on fainter sources

- the AO system can run faster

I will show in the next slides that it is not possible to get all 3 properties simultaneously, and the WFS needs to be carefully chosen to fit the AO system requirements.

Wavefront Sensor Options...

Linearity, dynamical range and sensitivity

Linear, large dynamical range, poor sensitivity: Shack-Hartmann (SH) Curvature (Curv) Modulated Pyramid (MPyr)

Linear, small dynamical range, high sensitivity: Fixed Pyramid (FPyr) Zernike phase constrast mask (ZPM) Pupil plane Mach-Zehnder interferometer (PPMZ)

Non-linear, moderate to large dynamical range, high sensitivity: Non-linear Curvature (nlCurv) Non-linear Pyramid (nlPyr) ?

High sensitivity WFS : Three examples

- **Fixed Pyramid WFS**: A pyramid is placed in the focal plane. The starlight hits the tip of the pyramid
- Zernike phase contrast: A small phase shifting mask is placed in the focal plane. Roughly 1/2 of the light goes through, 1/2 goes around. The two halves interfere to give an intensity signal
- Mach-Zehnder / Self-referencing interferometer / point diffraction interferometer: An interferometer is assembled by splitting the beam in 2 and recombining the two halves. On one of the arms, a spatial filter (pinhole) is placed to create the "reference" beam which interferes with the wavefront
- These 3 options are Linear but will fail (or loose sensitivity) if there is more than ~ 1 rad of WF error ! -> poor dynamical range

Sensitivity: how to optimally convert a phase error into an intensity signal ?

Example: a sine wave phase aberration of C cycles across the pupil, amplitude = a rad (in figure below, C = 3, a = 1 rad)

Interferences between points separated by x (2xC PI in "phase" along the sine wave)

Phase difference between 2 points: phi = 2 a sin(xC PI)

Intensity signal is linear with phi (small aberrations approximation)

For a sine wave aberration on the pupil, a good WFS will make interferences between points separated by ~ half a period of the sine wave

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SH WFS : sensitivity issue for low spatial frequencies



Problem:

SH does not allow

interferences between points of the pupil separated by more than subaperture size

 Poor sensitivity to low order modes ("noise propagation" effect)

This gets worse as the number of actuators increases !!!



Curvature WFS

Light propagation turns phase into amplitude (similar to scintillation)



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Curvature WFS

Wavefront Signal.

The optimal defocus distance at which the measured signal is strongest, is larger for lower spatial frequencies. For high spatial frequencies the linear domain extends to ~ 500 km.





Reconstruction Algorithm



Reconstruction Algorithm

For faster reconstruction:

- (1) bin down data to low resolution and run iterative algorithm
- (2) expand solution to full resolution and run a small number of iterations
- (3) Speed up convergence by injecting derivative between iterations

Iterative loop is slow, but:

- Linear algorithm can give fast low sensitivity estimate used as starting point
- Locally linear (within 1 rad)
- Becomes linear if aberration < 1 rad (valid for high performance AO closed loop)

Faster hardware coming online (GPUs)

Wavefront sensing at the diffraction limit of the telescope



Fig. 9.— Wavefront reconstruction using the algorithm shown in fig. 8. Four noisy defocused pupil images (images (a), (b), (c) and (d)) are acquired to transform the pupil phase aberrations (e) into intensity signals. The input pupil phase is 609 nm RMS, yielding the PSF (f) before correction. After correction, the residual pupil phase aberration (g) is 34.4 nm RMS, allowing high Strehl ratio imaging (h). All images in this figure were obtained at 0.65 μ m. The total number of photons available for wavefront sensing in 2e4.

Computer Simulations showing contrast gain with high sensitivity WFS (nonlinear curvature)

m ~ 13

WFS

nlCurv

SH - D/9

SH - D/18

SH - D/36

	LOOP OFF	7	SH, D/d = 60 Loop frequency = 140 Hz	SH, D/d = 36 Loop frequency = 160 Hz
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ain				
,		1537 nm RMS	227 nm RMS	183 nm RMS
-	SH, D/d = 18 Loop frequenc	ey = 180 Hz	SH, D/d = 9 Loop frequency = 180 Hz	nlC, limit = 16 CPA Loop frequency = 260 Hz
)				
•				
3		195 nm RMS	315 nm RMS	101 nm RMS
	Loop frequ	RMS	SR @ 0.85 un	n SR @ 1.6 um
	260 Hz	101 nm	57%	85%
	180 Hz	315 nm	~4%	22%
	180 Hz	195 nm	~13%	56%
	160 Hz	183 nm	~16%	60% ₁₃
	1/0 Hz	227 nm	~6%	15%



Fig. 9.— Wavefront reconstruction with dual stroke non-linear CWFS on a sparse pupil. The pupil amplitude (a) and phase (b) yield the four defocused pupil images shown on the right. The recovered pupil phase (c) and the residual phase error (d) demonstrate that dual stroke non-linear CWFS can simultaneously measure OPD within and across segments. This polychromatic simulation was performed with 2e8 photons in a $d\lambda/\lambda = 0.5$ wide band centered at 0.65 μm .

"High Sensitivity Wavefront Sensing with a non-linear Curvature Wavefront Sensor", Guyon, O. PASP, 122, pp.49-62 (2010)

Sensitivity

Wavefront sensor sensitivity: definition

Sensitivity = how well each photon is used

For a single spatial frequency (OPD sine wave in the pupil plane, speckle in the focal plane):

Error (rad) = Sensitivity / sqrt(# of photons)

IDEAL WFS: Sensitivity Beta = 1 (1 ph = 1 rad of error) At all spatial frequencies <u>Non-ideal WFS:</u> Beta > 1 (Beta x Beta ph = 1 rad of error)

Wavefront sensors "sensitivities" in linear regime with full coherence (Guyon 2005)



Square root of # of photons required to reach fixed sensing accuracy

plotted here for phase aberrations only, 8m telescope. Tuned for maximum sensitivity at 0.5"from central star.

Figure above shows sensitivity (y axis) as a function of pupil spatial frequency (x axis). Pupil spatial frequency = angular separation in focal plane.

ALL wavefront sensor options have very good sensitivity at the spatial frequency defined by the WFS sampling SOME wavefront sensors loose sensitivity at low spatial frequencies (red), other do not (blue)

Sensitivity compared with other schemes



Performance gain for ExAO on 8-m telescopes



"High Sensitivity Wavefront Sensing with a non-linear Curvature Wavefront Sensor", Guyon, O. PASP, 122, pp.49-62 (2010)

Large gain at small angular separation: ideal for ExAO

Wavefront sensing at the sensitivity limit imposed by the telescope diffraction limit

Seeing limited wavefront sensing (what we do now) Example: SH WFS

Diffraction limited wavefront sensing (what needs to be done for ExAO)

Examples: Pyramid (non-modulated), non-linear curvature

Tip-tilt example (same argument applicable to other modes): With low coherence seeing-limited WFS, $\sigma^2 \sim 1/D^2$ (more photons) Ideally, one should be able to achieve: $\sigma^2 \sim 1/D^4$ (more photons + smaller λ/D)

This makes a big difference for Extreme-AO on large telescopes

For Tip-Tilt, SHWFS on ELT is 40000x less sensitive than diffraction-limited WFS (11.5 mag) Similar gain on other low order modes

Chromaticity



Chromaticity



8 m diameter pupil 371 nm RMS





Fig. 6.— Top: Closed loop 1 second exposure PSFs at 0.85 μ m with a nlCWFS working in monochromatic and broadband (d λ/λ = 40%) light. In both simulations, the total number of photons in the nlCWFS is 3e6 ph/s. Bottom: Without chromatic correction within the nl-CWFS (replacing the chromatic lenses by achromatic lenses in Figure 1), the loop would be unstable with d λ/λ =0.2.

Chromaticity compensation

Simulation results

Monochromatic algorithm Polychromatic data

Chromaticity compensation with chromatic optics



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Optical implementation



Better solution (suggested by Marcos Van Dam): split 4 beams according to wavelength with dichroics

 \rightarrow mitigates (solves ?) chromaticity issue (to be simulated and validated)

Faint source regime



Fig. 7.— Simulated obtained with a non-li based AO system. Th μ m for this simulation

Fig. 8.— Simulated performance of a low order nlCWFS-based system (first 200 Zernike modes corrected) as a function of sensing wavelength (0.7, 0.85 and 1.0 μ m) and guide star brightness. The stellar magnitudes given in this figure assume a 20% efficiency in a 0.5 μ m wide band. Each point in this figure is a 1-second average of the RMS residual wavefront error. See text for details.

Extended sources

Extended source:

- \rightarrow no diffraction limited speckles
- \rightarrow sensitivity loss



Example: seeing-limited source (Laser Guide Star) \rightarrow no gain beyond SH WFS

However, nICWFS should be beneficial for extended source with fine structure

 \rightarrow simultaneous wavefront + source estimation required

Lab validation

Light

source

Dual arm: nICWFS + SHWFS

SHWFS camera

nlCWFS camera

Wavefront reconstruction

Data acquired in the lab



Gerchberg-Saxton solution



Sensitivity measurement using lab data





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Conclusions

The nICWFS concept offers high sensitivity without requiring high quality wavefront \rightarrow attractive for adaptive optics

Can fully exploit the telescope diffraction limit in a wide range of conditions

- Star brighter that mV~15
- Natural guide star (or possibly extended object with structure)

 \rightarrow nICWFS greatly improves sensitivity for NGS, and for low-order aberrations, makes NGS as good a target as LGS ~1000x to 10000x brighter on large telescopes

Challenges are **computing power** for reconstruction and chromaticity

Lab demonstration ongoing, plans to install on ground-based telescope

For more info on the concept:

"High Sensitivity Wavefront Sensing with a non-linear Curvature Wavefront Sensor", Guyon, O. PASP, 122, pp.49-62 (2010) 30