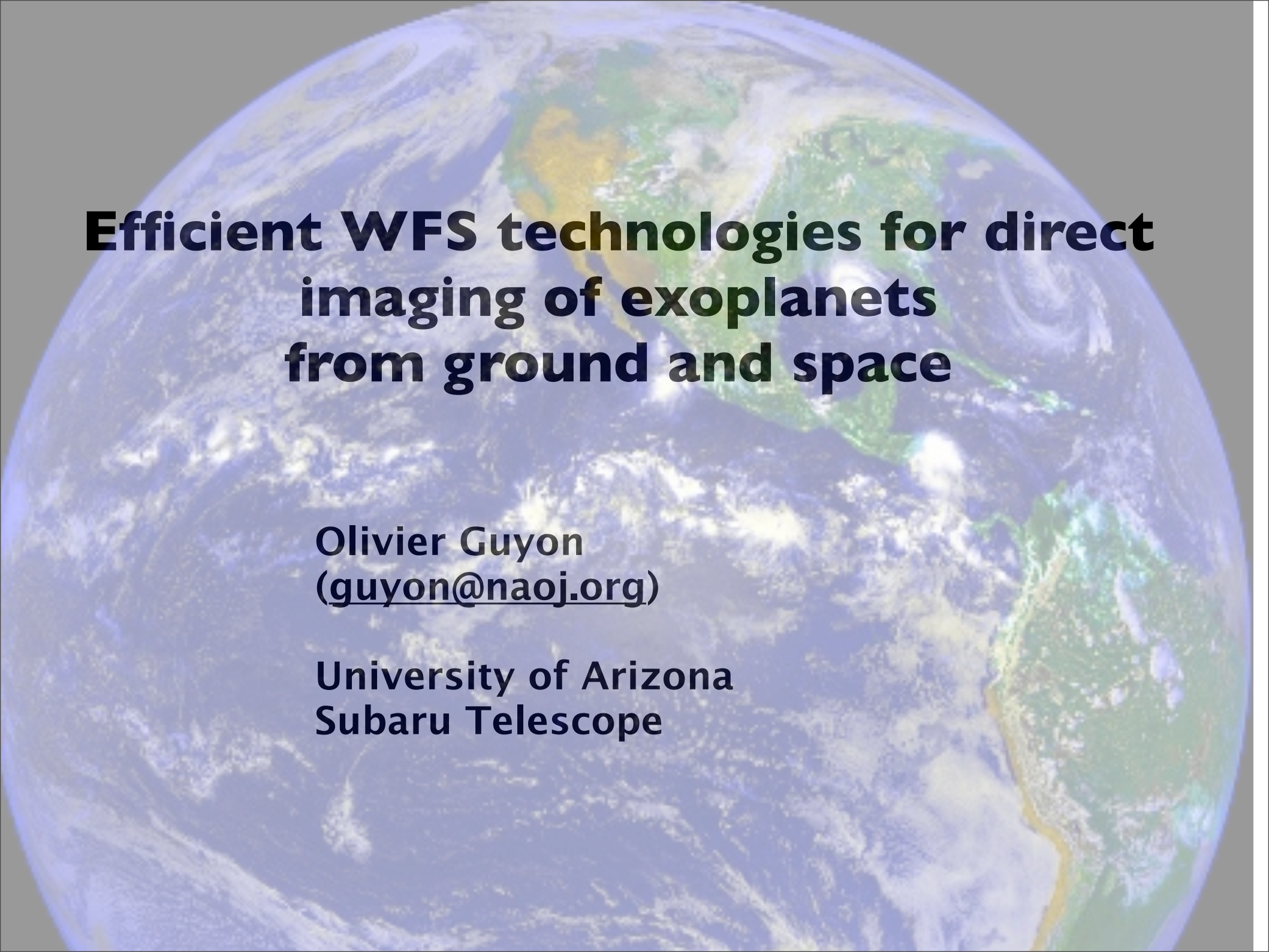




Efficient WFS technologies for direct imaging of exoplanets from ground and space

Olivier Guyon
(guyon@naoj.org)

University of Arizona
Subaru Telescope

Wavefront Sensor Options...

Linear, large dynamical range, poor sensitivity:

Shack-Hartmann (SH)

Curvature (Curv)

Modulated Pyramid (MPyr)

Linear, small dynamical range, high sensitivity:

Fixed Pyramid (FPyr)

Zernike phase contrast mask (ZPM)

Pupil plane Mach-Zehnder interferometer (PPMZ)

Non-linear, moderate to large dynamical range, high sensitivity:

Focal Plane (FP)

Non-linear Curvature (nlCurv)

Non-linear Pyramid (nlPyr) ?

Next slide compiles strengths and weaknesses of WFS options, and will be explained with simple but fundamental physics ...

	sensitivity	range	Extended target ? (LGS)	chromaticity	maturity	detector use
SH	serious noise propagation	Very good	Yes	Low	on sky	at least 4 pixels per subaperture
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Non-linear curvature	Excellent	Good, can have > 1 rad error, but needs coherence	No	Low	in lab with no turbulence	4 pix/subaperture

Wavefront sensor sensitivity

Sensitivity = how well each photon is used

For a single spatial frequency (OPD sine wave in the pupil plane, speckle in the focal plane):

Error (rad) = Sensitivity / sqrt(# of photons)

IDEAL WFS:

Sensitivity Beta = 1 (1 ph = 1 rad of error)

At all spatial frequencies

Non-ideal WFS:

Beta > 1 (Beta x Beta ph = 1 rad of error)

How to optimally convert phase into an intensity signal ?

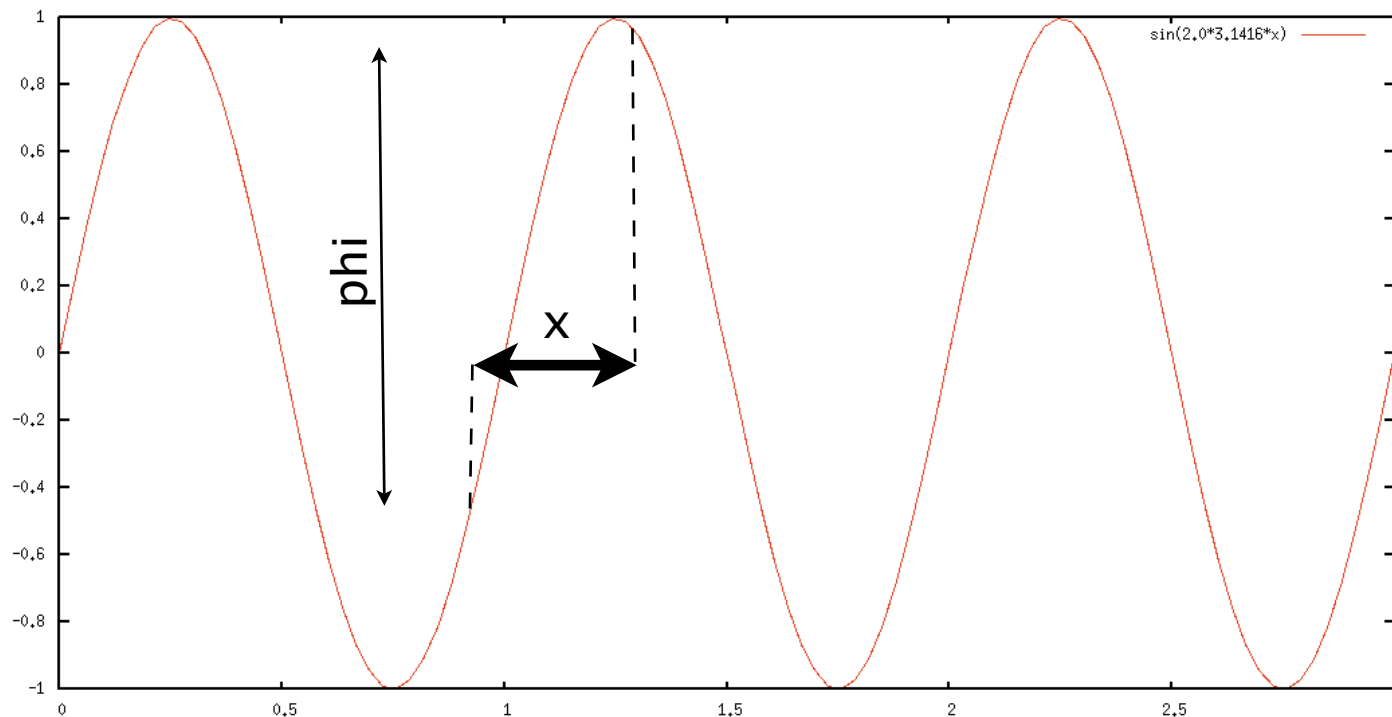
Example: a sine wave phase aberration of C cycles across the pupil, amplitude = a rad (in figure below, $C = 3$, $a = 1$ rad)

Interferences between points separated by x ($2xC$ PI in “phase” along the sine wave)

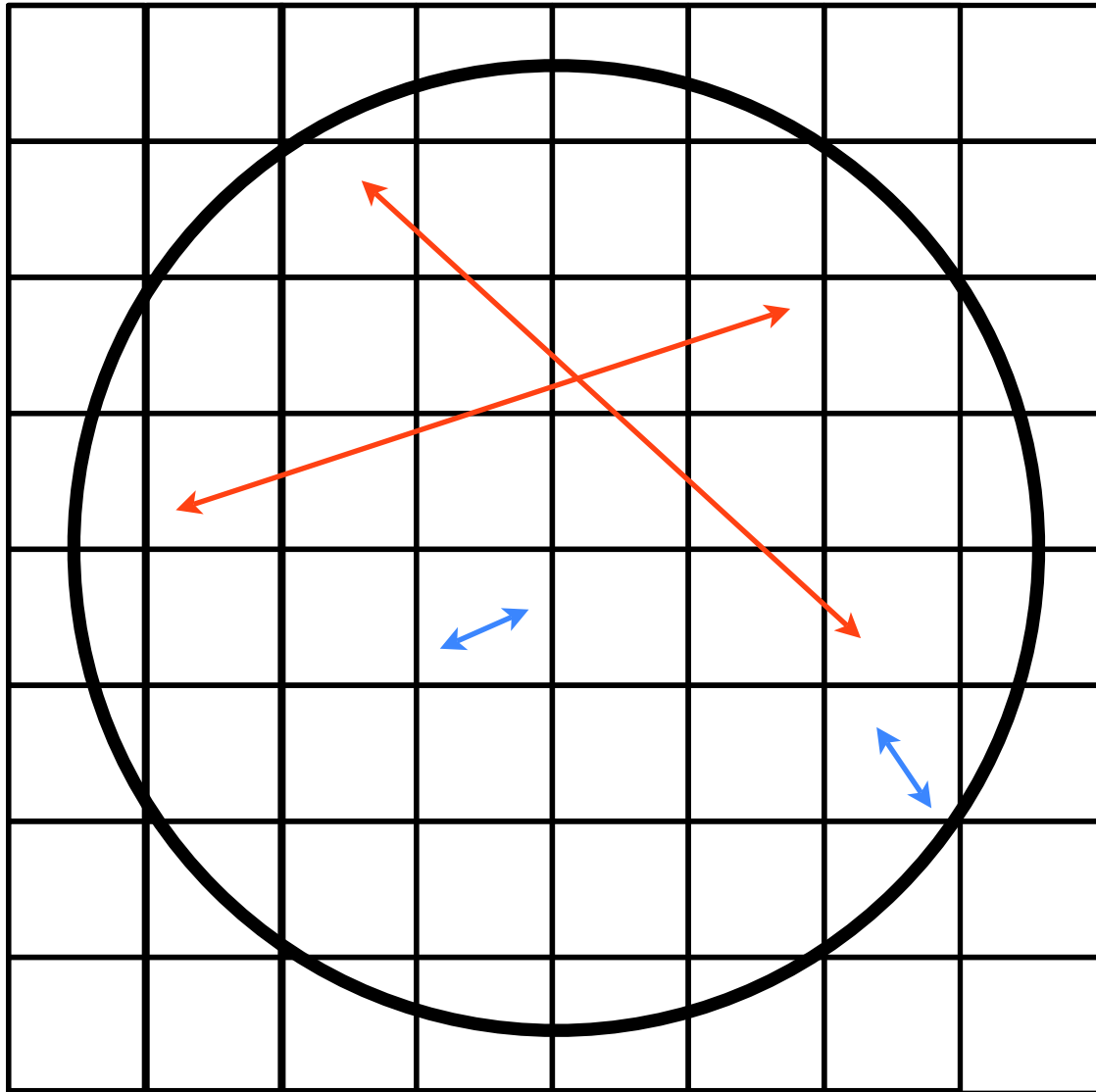
Phase difference between 2 points: $\phi = 2 a \sin(xC \text{ PI})$

Intensity signal is linear with ϕ (small aberrations approximation)

For a sine wave aberration on the pupil, a good WFS will make interferences between points separated by $\sim$ half a period of the sine wave



SH WFS : sensitivity



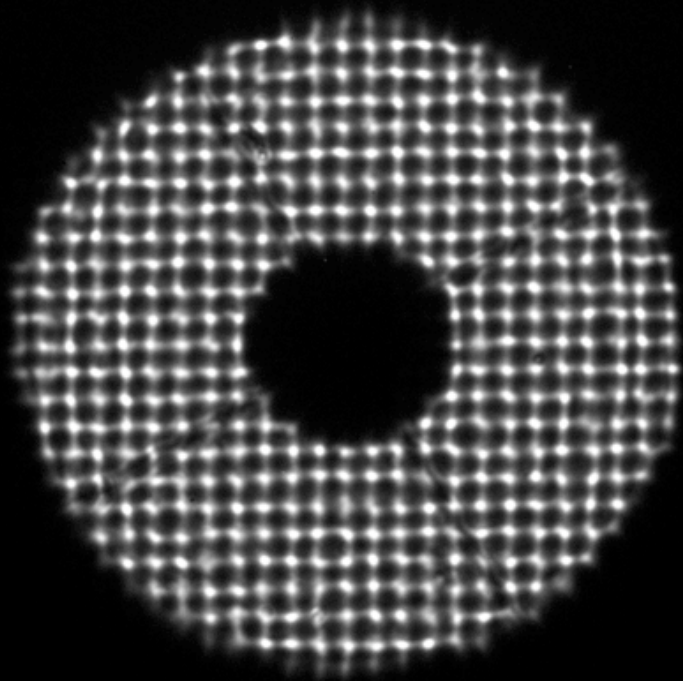
Problem:

SH does not allow interferences between points of the pupil separated by more than subaperture size

→ Poor sensitivity to low order modes (“noise propagation” effect)

This gets worse as the number of actuators increases !!!

SH WFS is also suffering from noise propagation



Spot sizes is λ/r_0 at best
(λ/d if $d < r_0$) $\gg \lambda/D$

Low order modes suffer from
very poor SNR

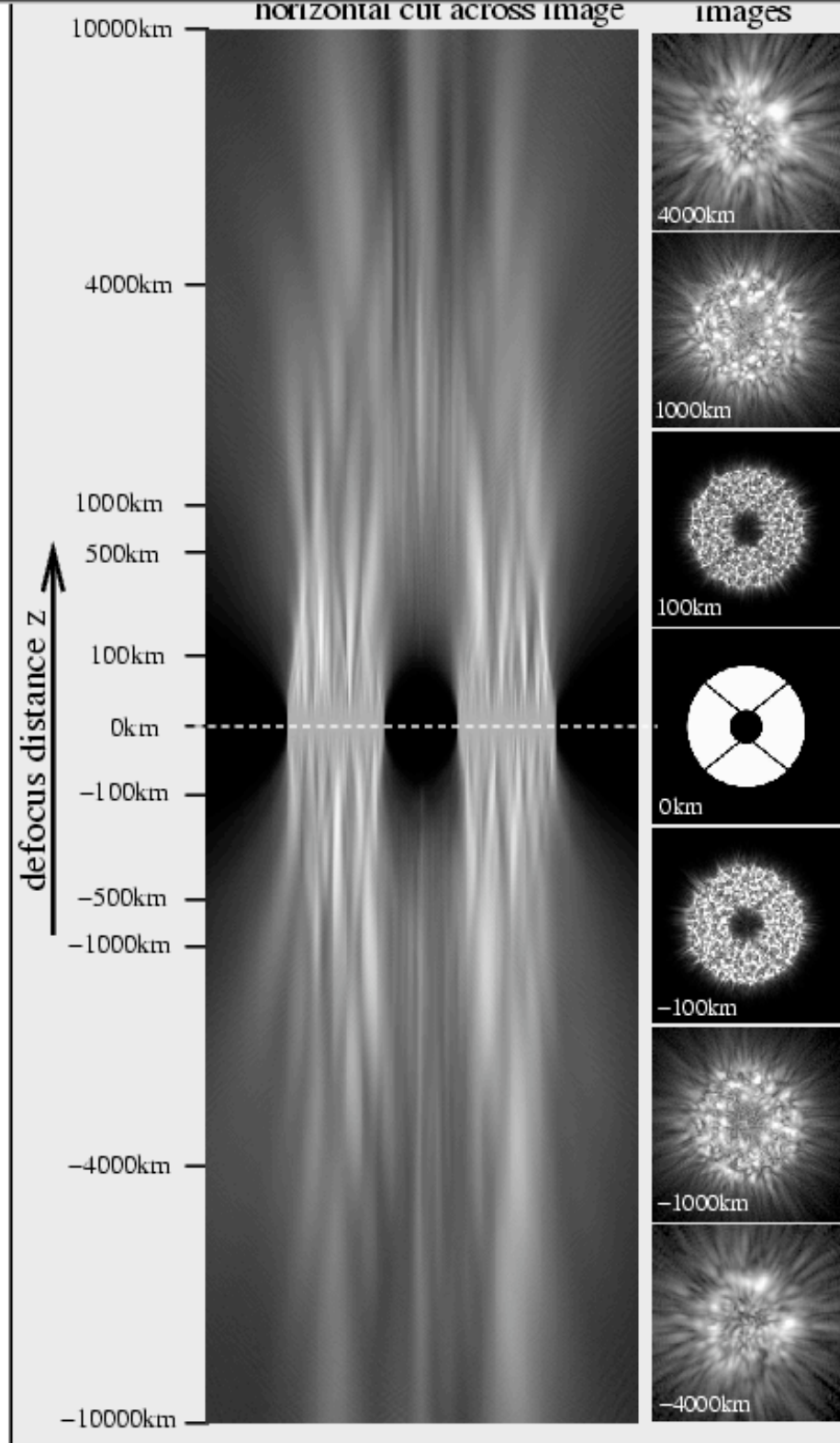
Curvature WFS

Uses **light propagation** to convert phase into intensity
→ measure intensity in at least 2 “defocused” pupil planes and compute phase.

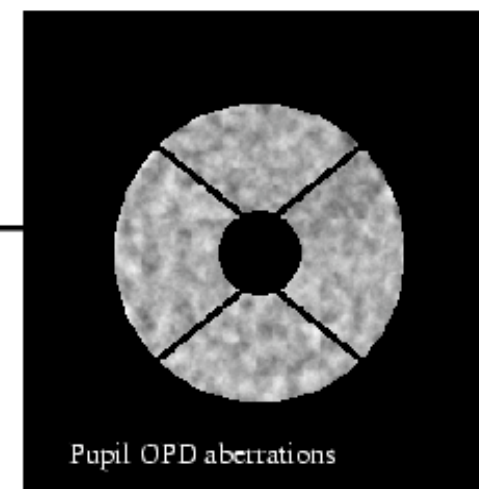
Usually, planes at $+dz$ and $-dz$, with $dz \sim 1000\text{km}$ are imaged.

If dz “small” ($\sim 1000\text{ km}$), **defocused images are linear function of wavefront curvature**

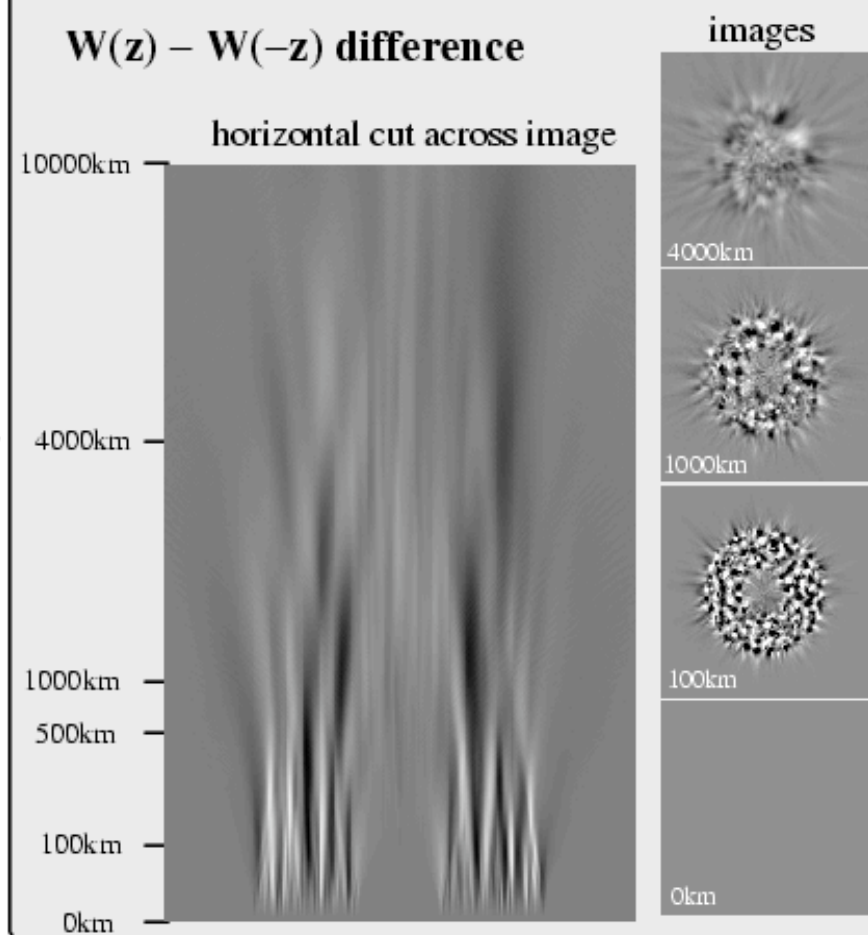
Future slides will show how phase is converted into intensity modulation in a CWFS



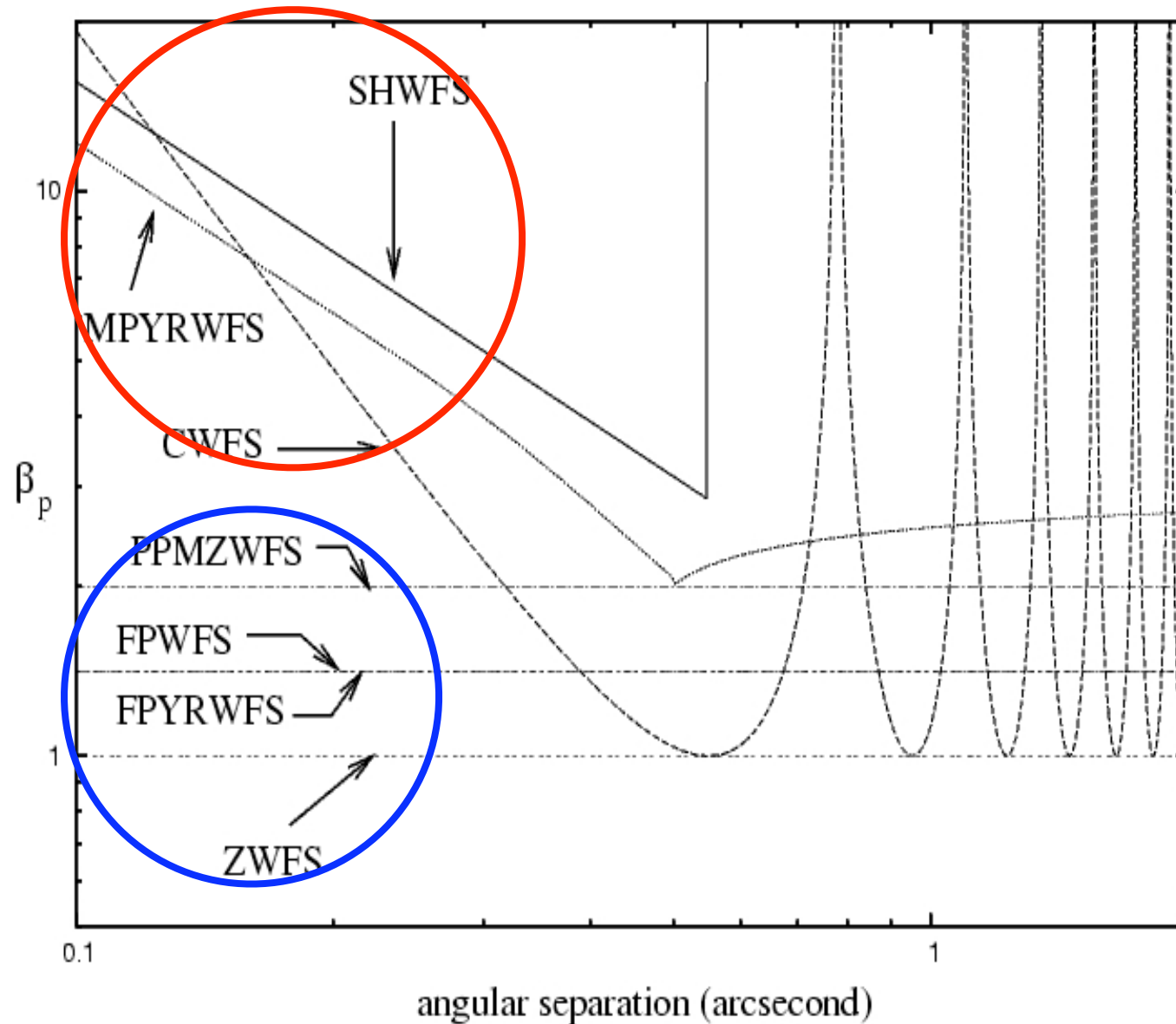
**$W(z)$
images**



$W(z) - W(-z)$ difference



Wavefront sensors "sensitivities" in linear regime with full coherence (Guyon 2005)



Square root of
of photons
required to reach
fixed sensing
accuracy

plotted here for
phase aberrations
only, 8m telescope.
Tuned for maximum
sensitivity at 0.5''
from central star.

Why do SH, Curvature (& modulated pyramid) have bad sensitivity for low order aberrations ?

Good measurement of low order aberrations requires interferometric combination of distant parts of the pupil
FPWFS does it, but:

- – SH chops pupil in little pieces → no hope !
- – Curvature has to keep extrapupil distance small (see previous slides) → same problem

Things get worse as # of actuators go up.

→ **This makes a big difference for ELTs**

Tip-tilt example (also true for other modes):

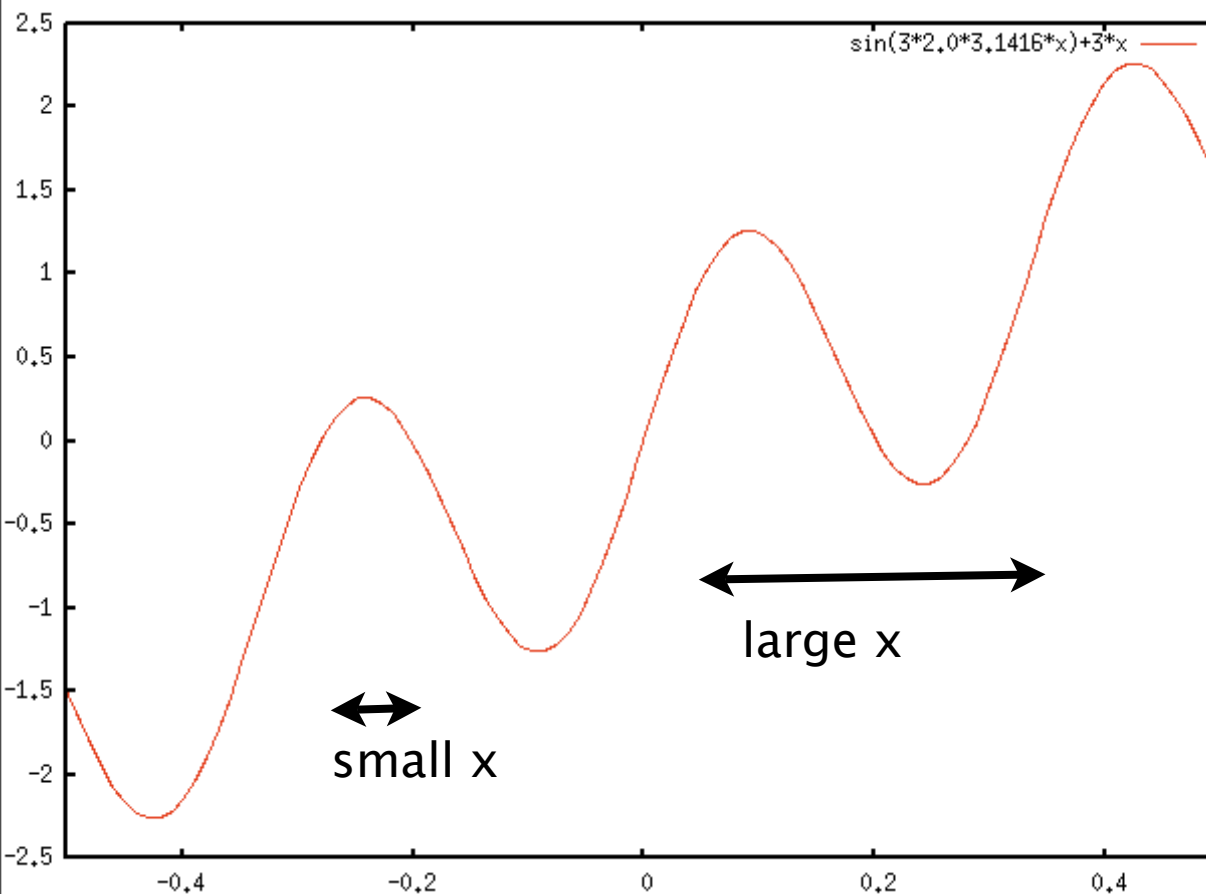
With low coherence WFS, $\sigma^2 \sim 1/D^2$ (more photons)

Ideally, one should be able to achieve:

$\sigma^2 \sim 1/D^4$ (more photons + smaller l/D)

	sensitivity	range	Extended target ? (LGS)	chromaticity	maturity	detector use
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WFS range / linearity



small x:
 $\phi < 1$ rad
WFS signal is linear with
phase aberrations

large x:
 $\phi > 1$ rad
WFS signal is non-linear
with phase aberrations

WFS range, linearity and WFS sensitivity are pushing the WFS architecture in opposite directions

Solution:

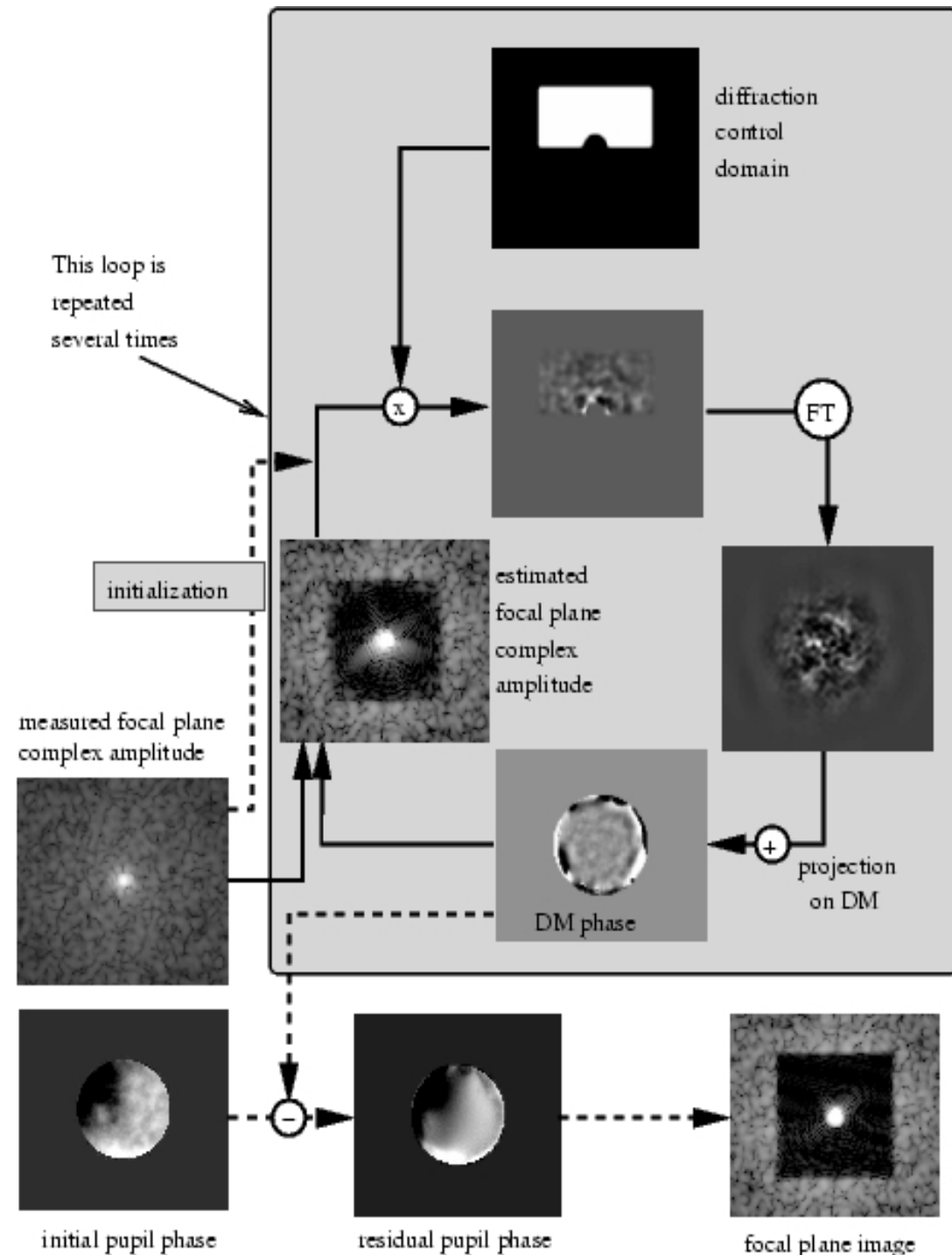
Non-linear reconstruction allows a large dynamical range measurement on a high-sensitivity WFS

Focal plane WFS

If speckle field Complex amplitude is known, **DM(s)** can be **controlled to "perfectly" cancel speckles**

DM can be also be asked to **create "arbitrary" speckle field for WFS**

Malbet, Yu & Shao (1995)
Guyon (2005)
Giv'oni (2003–2006)
Borde & Traub (2006)



	sensitivity	range	Extended target ? (LGS)	chromaticity	maturity	detector use
SH	serious noise propagation	Very good	Yes	Low	on sky	at least 4 pixels per subaperture
Curvature	serious noise propagation	Very good	Good range/linearity but poor sensitivity			1 pix/subaperture 2 reads
Pyramid (modulated)	noise propagation	very good	Somewhat LGS OK	Low	on sky	4 pix/subaperture
Pyramid (fixed)	Excellent	limited to < 1 rad in closed loop	No	Low	closed loop lab AO w turbulence	4 pix/subaperture
Zernike phase contrast	Excellent	limited to < 1 rad in closed loop	Good sensitivity over a small range			1 pix/subaperture
Mach-Zehnder	Excellent	limited to < 1 rad in closed loop	No	low if near zero OPD	?	2 pix/subaperture
Focal plane	Excellent	Good, can have > 1 rad error, but needs coherence	No	serious	closed loop lab AO no turbulence	4 pix/speckle
Non-linear curvature	Excellent	Good, can have > 1 rad error, but needs coherence	Non-linear reconstruction algorithm allows good sensitivity and larger range			4 pix/subaperture

Guide “star” for WFS: COHERENCE

COHERENCE = ability to make coherent interferences between different parts of the pupil

Coherence is usually high across small parts of the pupil, low across large parts of the pupil

What makes the guide star “incoherent” ?

Wavefront stability during sampling time

- sampling time too long / turbulence too fast
- sensing wavelength too short
- vibrations

Large time-variable and/or unknown wavefront errors

- poor correction
- open loop wavefront sensing

Angular size of source

- Atmospheric dispersion
- source resolved $> \lambda/D$

Chromaticity

Wavefront coherence on large spatial scales must be maintained for high-sensitivity WFS

Temporal coherence:

“long WFS exposure” will greatly attenuate the signal

Limits the WFS sensitivity in low light level, where long WFS exposure is required

Spatial coherence:

Sensitivity will not be achieved on extended targets

Extended target = points separated by large distance in the pupil plane will produce weak interference

This is fundamentally same thing as saying that TT on an extended target is less sensitive

Fundamental effect, will limit all WFS designs equally

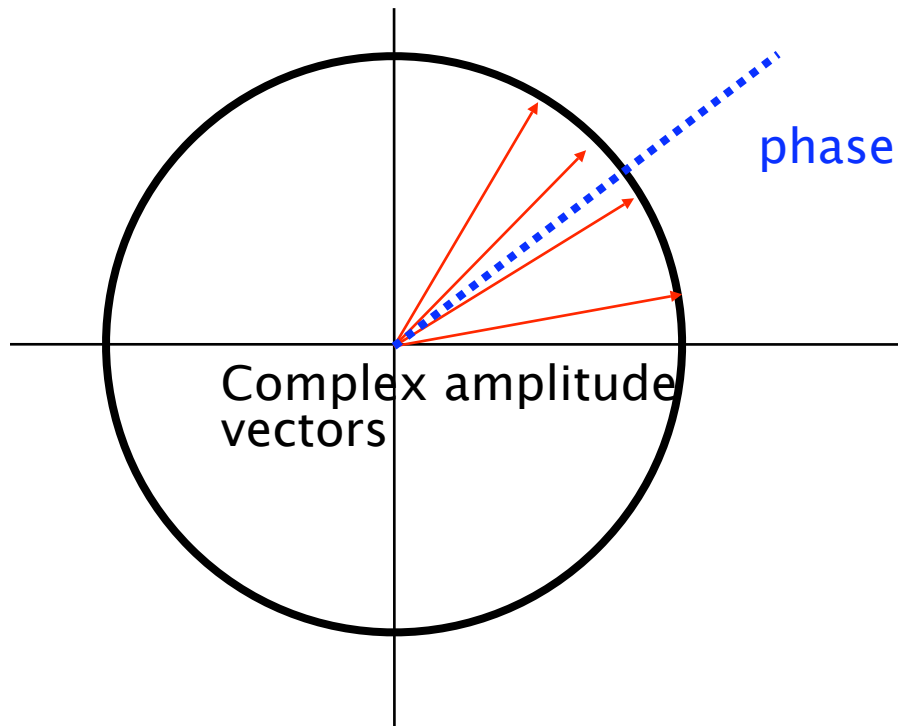
Chromatic coherence:

WFS design must work in broadband

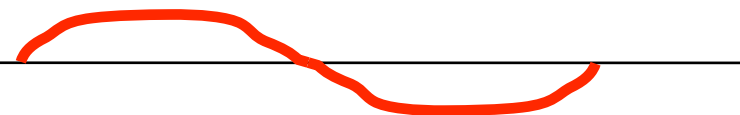
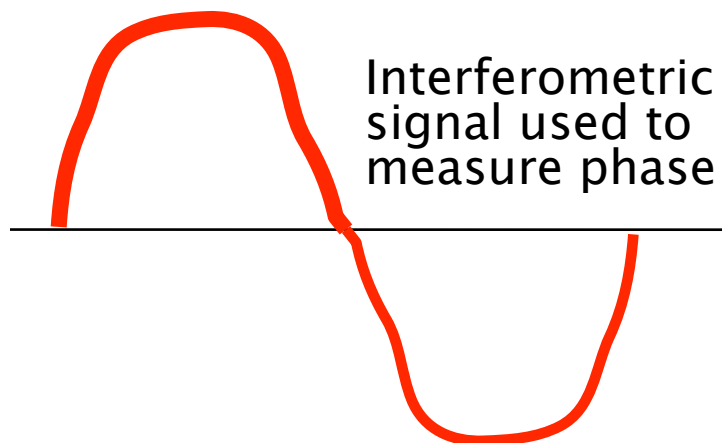
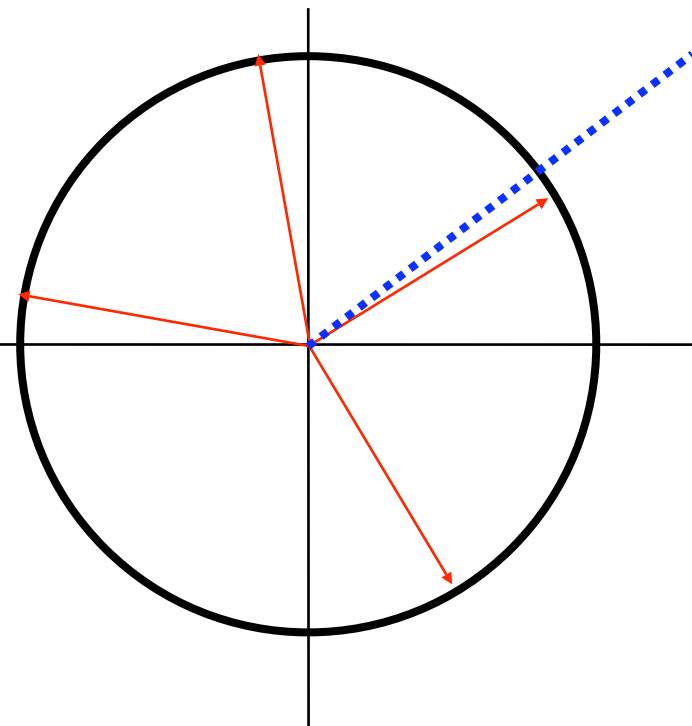
Problem for focal plane WFS, other WFS concepts can work in broadband

“interferometer” representation of temporal coherence in WFS

High coherence



Low coherence



Matching:

Wavefront COHERENCE
in WFS

to

Wavefront sensor

$\ll 1$ rad

Space Extreme-AO
(Terrestrial Planet Finder)

Second-stage of Extreme-AO
system in near-IR ("Tweeter")

Interferometric

Focal plane

~ 1 rad

Extreme-AO Closed loop in Visible

Thermal IR AO on 8m telescope
open loop

"general purpose" AO system in
closed loop

Not allowed

Pyramid (fixed)

allowed

Pyramid (modulated)

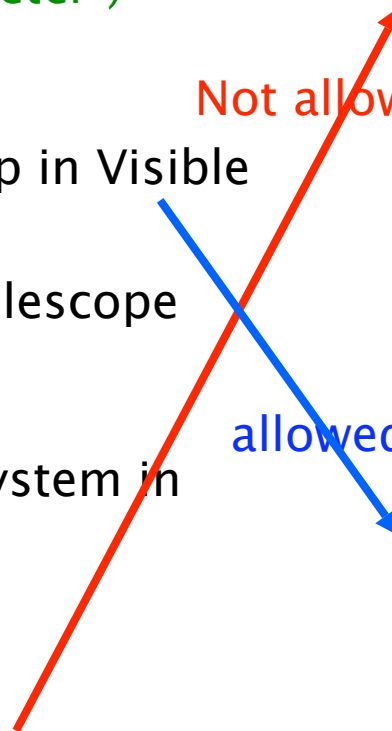
$\gg 1$ rad

LGS AO
GLAO

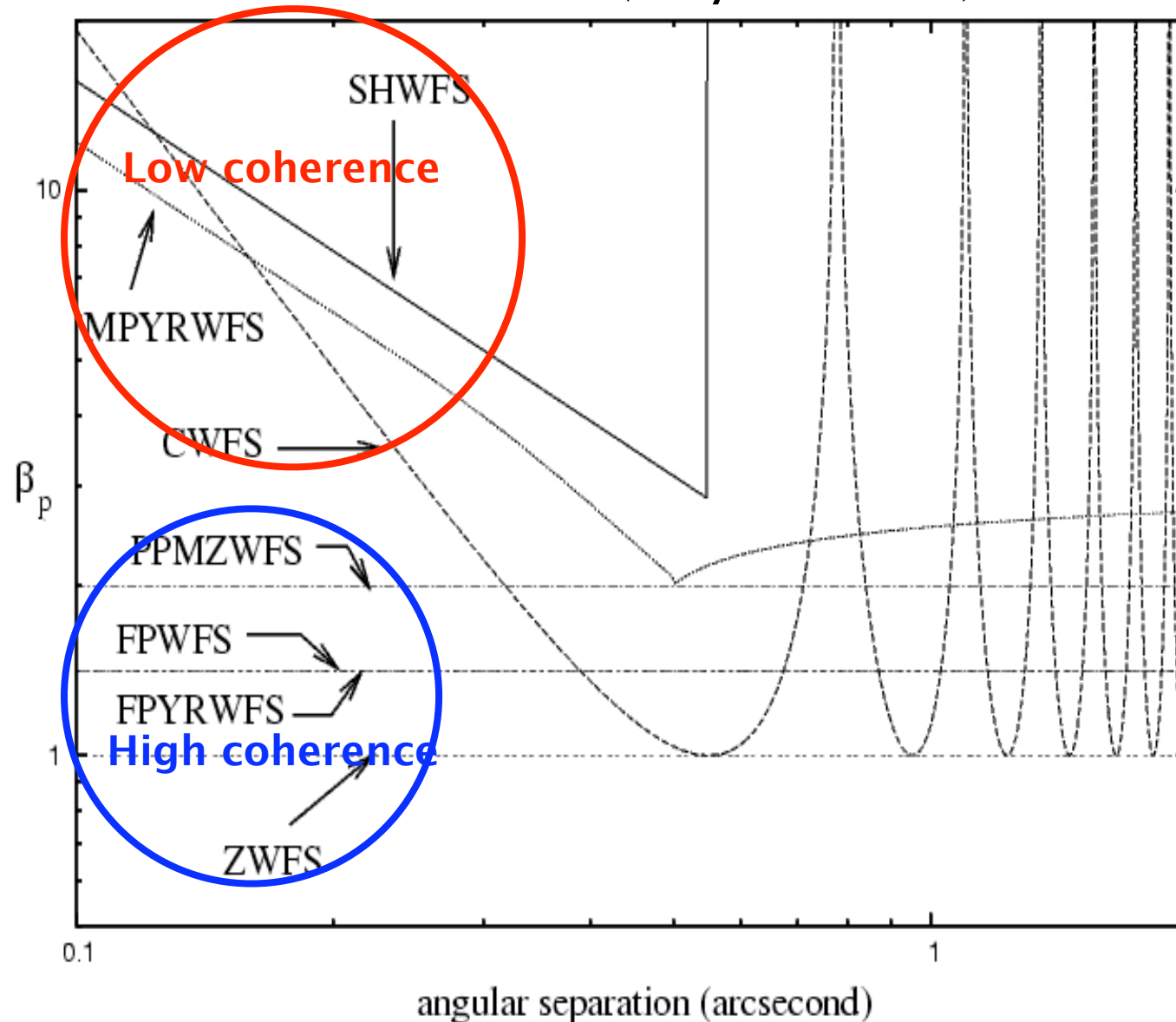
Open loop AO

Curvature

Shack-Hartmann



Wavefront sensors "sensitivities" in linear regime with full coherence (Guyon 2005)

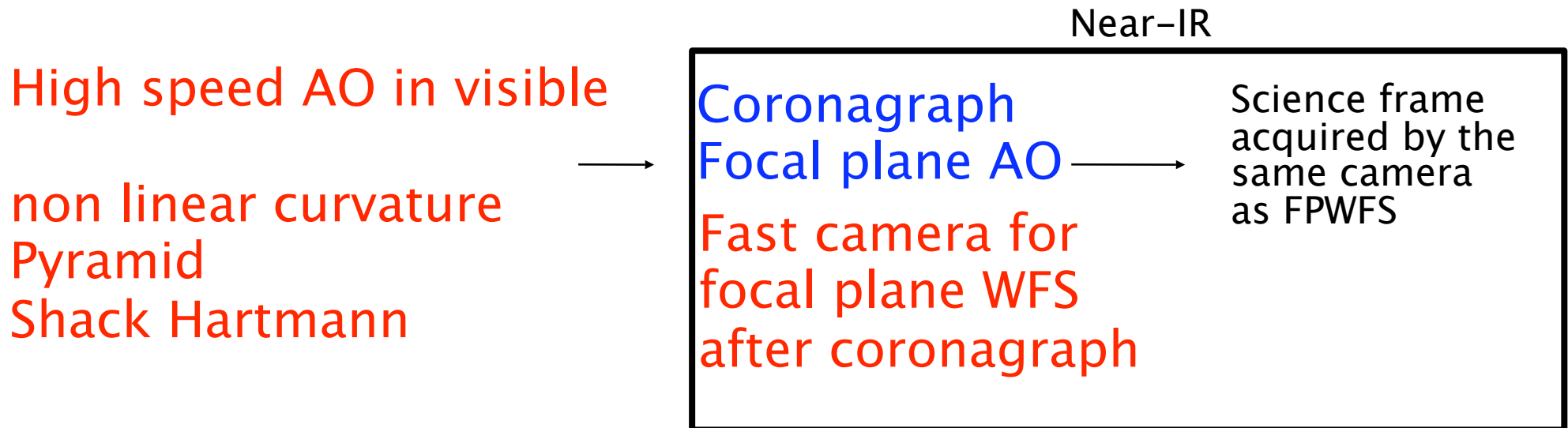


Square root of
of photons
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fixed sensing
accuracy

plotted here for
phase aberrations
only, 8m telescope.
Tuned for 0.5"
separation.

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Example: Possible Coronagraphic ExAO architecture

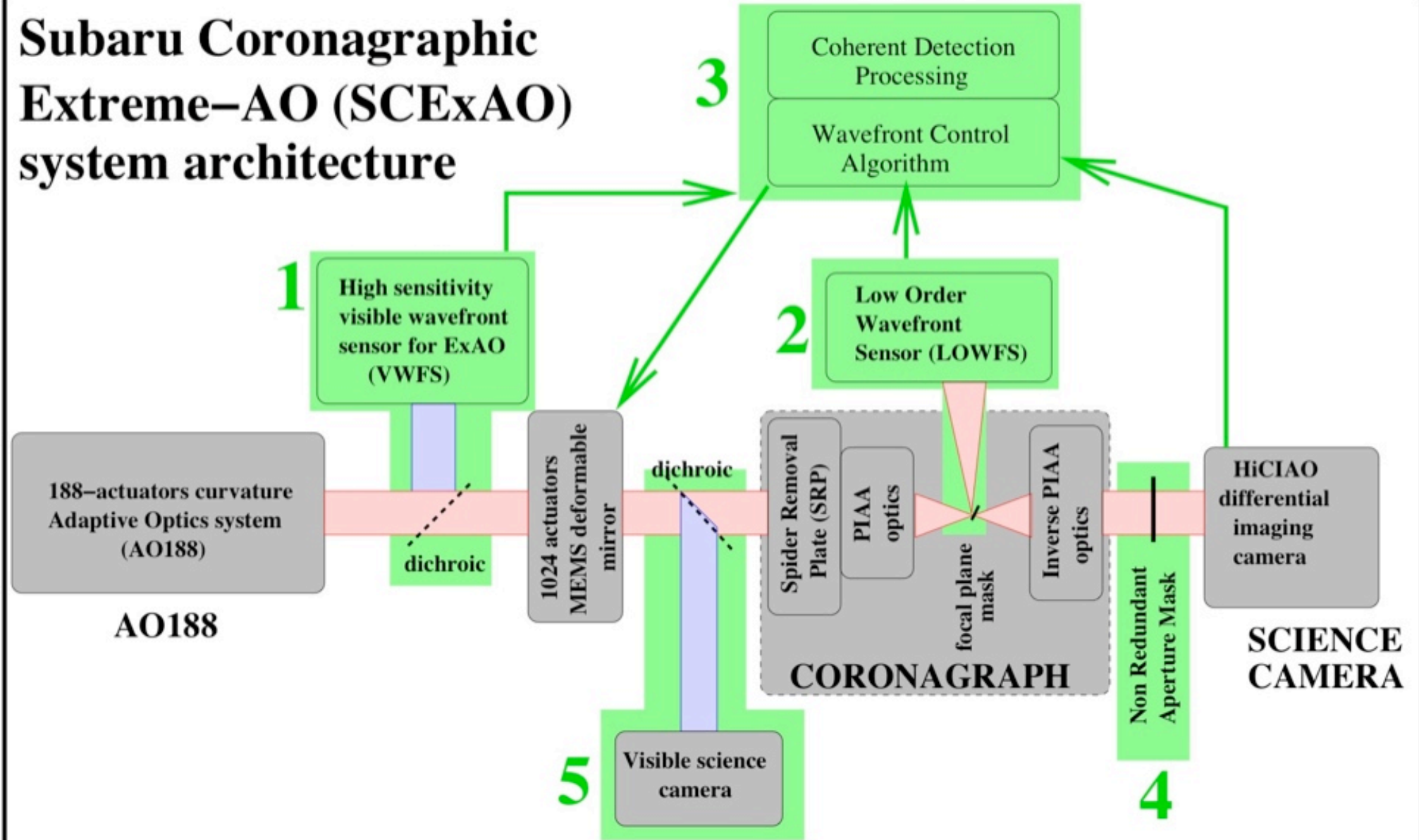


The first step is used to clean the wavefront within ~ 1 rad in Visible

The second step operates in the high coherence regime, and adopts the FPWFS.

Gemini Planet Imager (GPI) uses a similar strategy, with an interferometer to measure coherent residuals

Subaru Coronagraphic Extreme-AO (SCExAO) system architecture



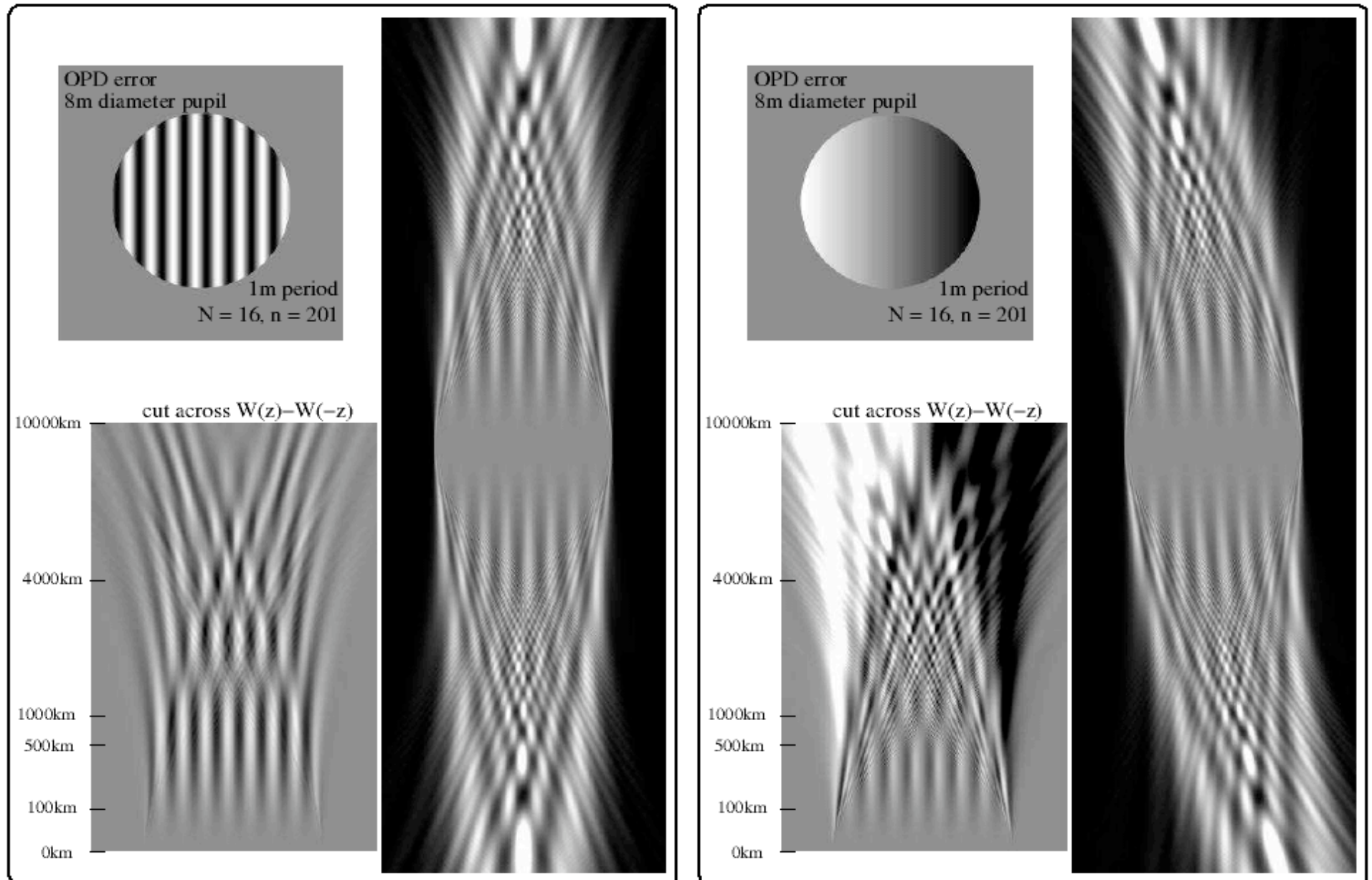
Non-linear Curvature WFS

SH: Noise propagation limitation is introduced at the optical level (chopping the pupil in small pieces)

Curvature: Noise propagation comes from processing of WFS frames, which imposes linearity

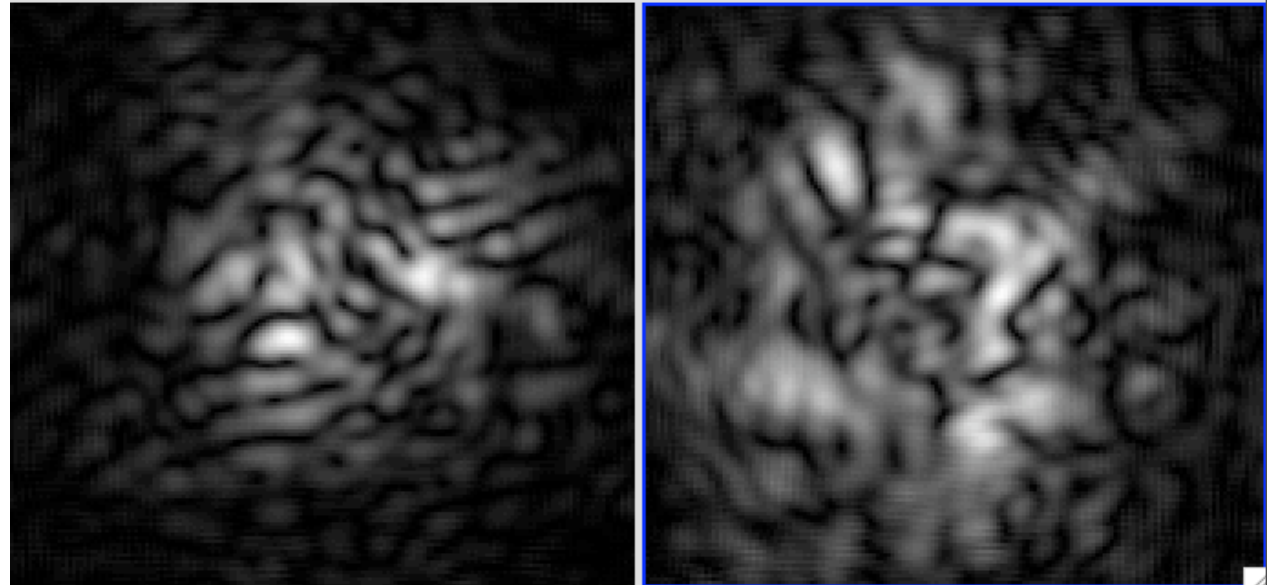
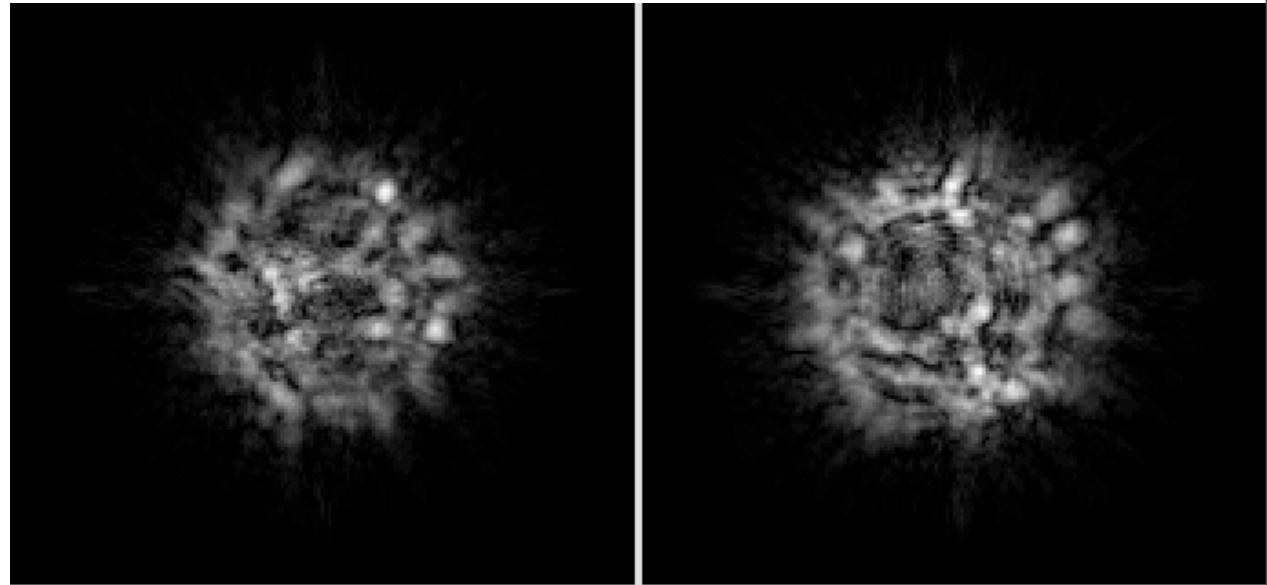
-> possible to mitigate / solve ?

Problem #2: Low order aberrations “scramble” high spatial frequencies
-> defocus distance must be kept small



Defocused pupil
images are full of
 λ/D speckles

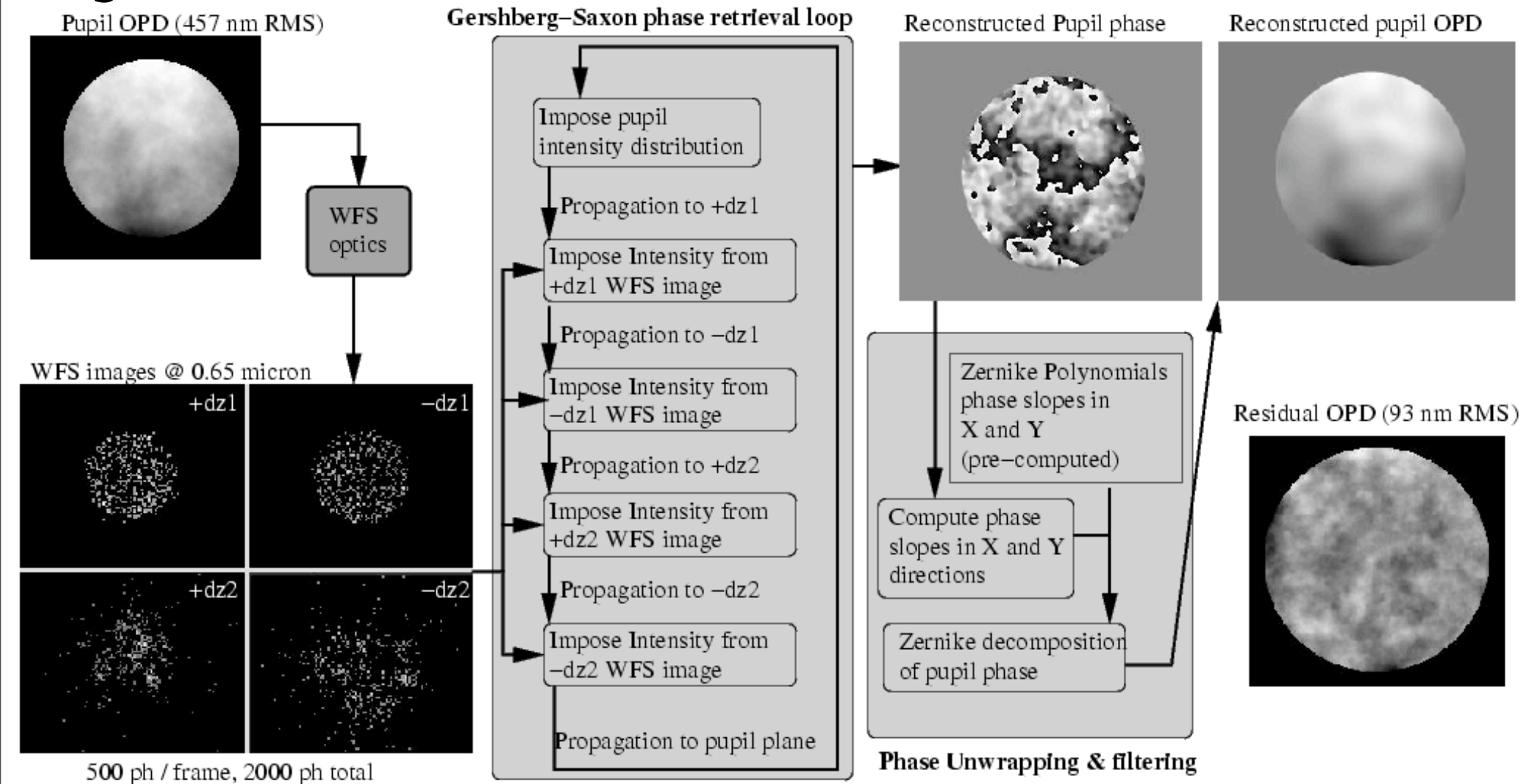
+/- 1000km



+/- 8000km

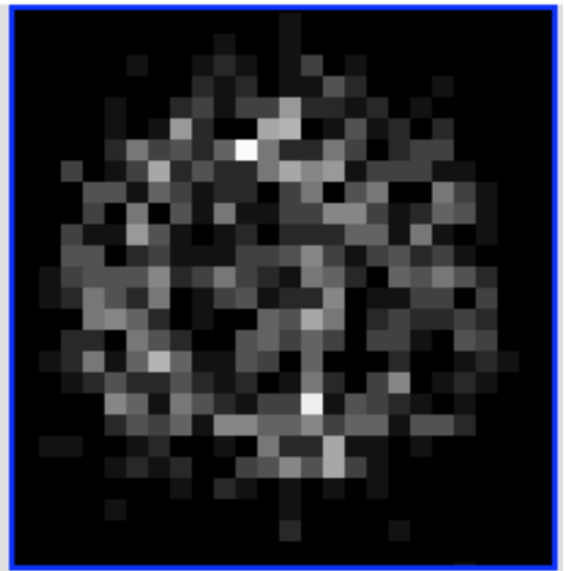
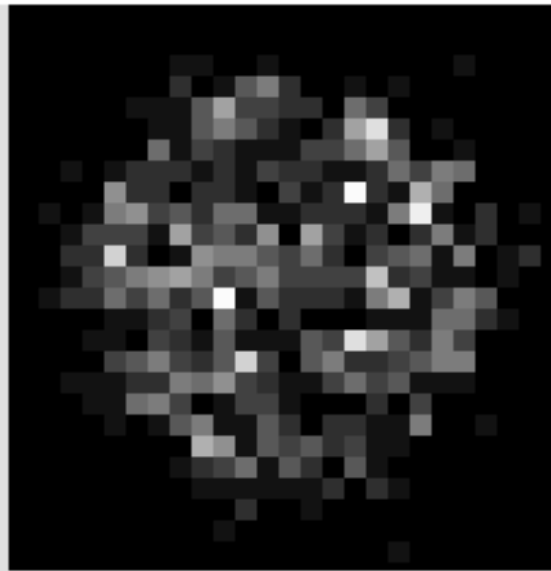
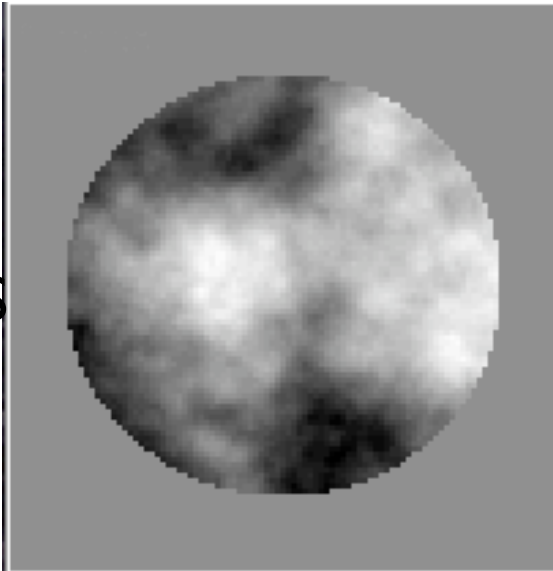
Standard phase diversity algorithm, working around pupil plane. There are probably better/faster algorithms (see for example: van Dam & Lane 2002, JOSA vol. 19)

kHz operation appears to be possible with current chips for few 100s actuators system (100 32x32pix FFT = 0.2ms on single CPU)

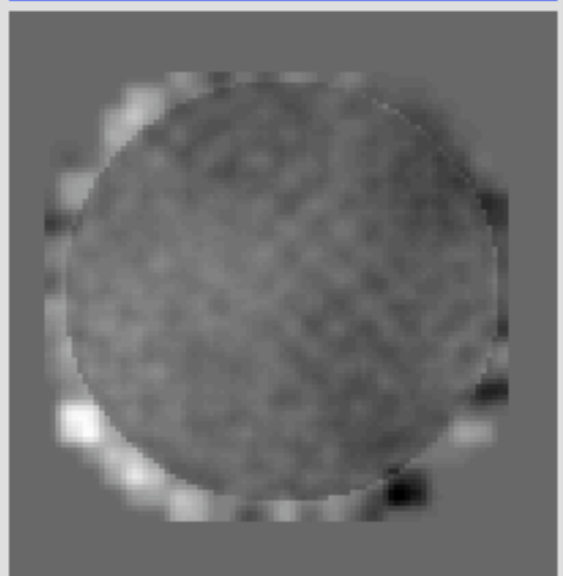
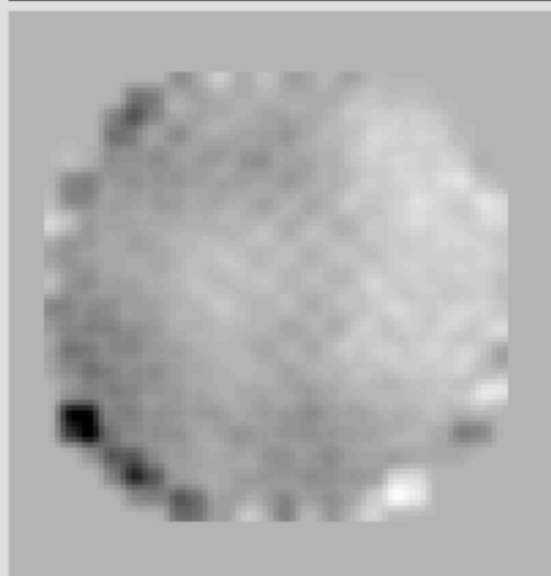
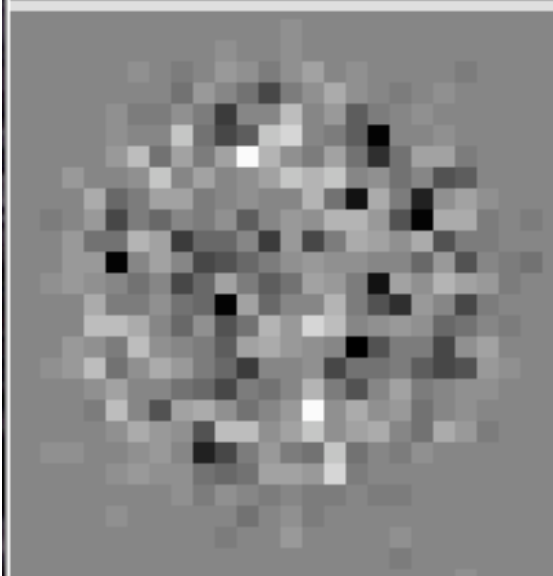


Linear single stroke WFS, 2000 ph total 8m telescope, 0.65 μ , 373 ill. subapert.

Input pupil
phase
296nm RMS



+/-
700km

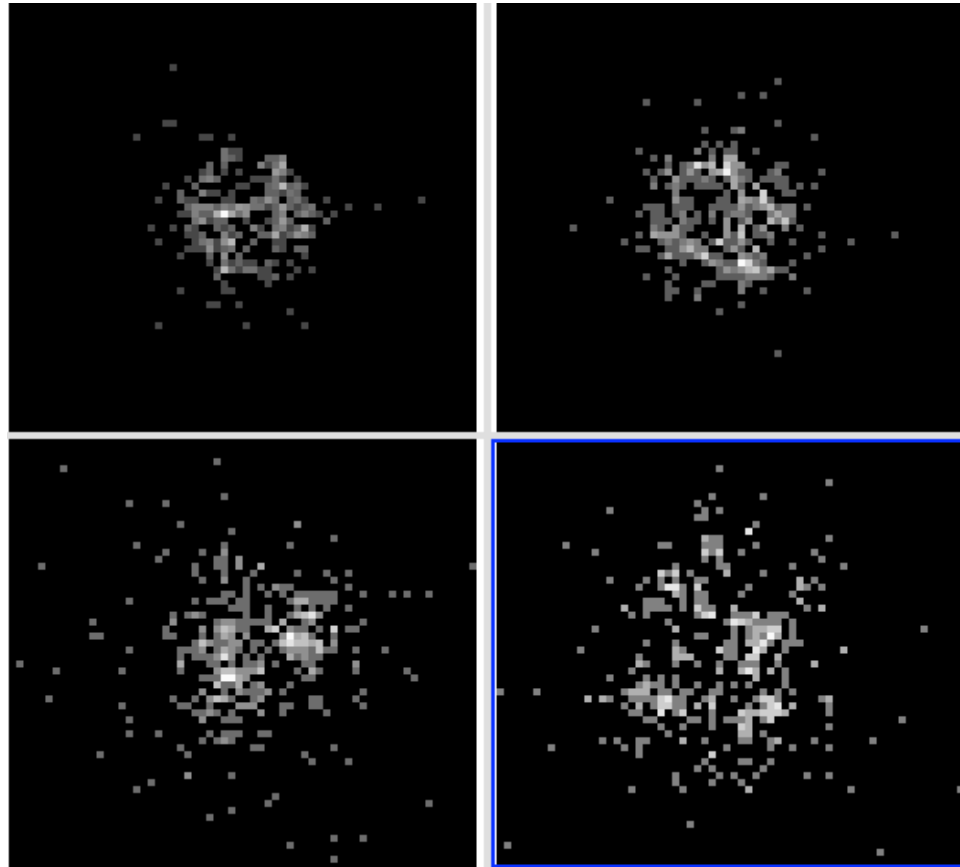


Curv. signal

Reconstructed phase

Residual: 196nm RMS

Non linear dual stroke WFS, 2000 ph total 8m telescope, 0.65 μ , 373 ill. subapert.



Defocused pupil images

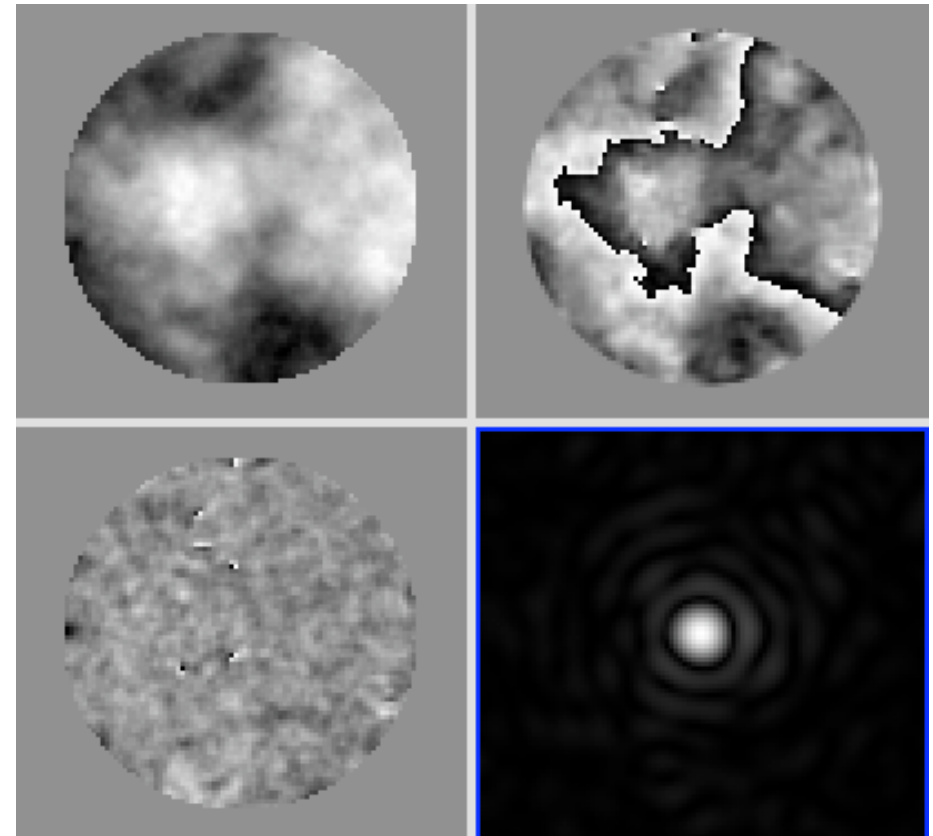
500 ph / frame

Top : ± 2000 km

Bottom: ± 8000 km

Input pupil phase
296nm RMS

Reconstructed
phase



Residual: 55nm RMS

SR = 0.763
at 0.65 micron

Magn 16 source $\rightarrow$ 2000 ph/ms on 8m
telescope

Why is it so good ??? -> uses HSF to infer LSF

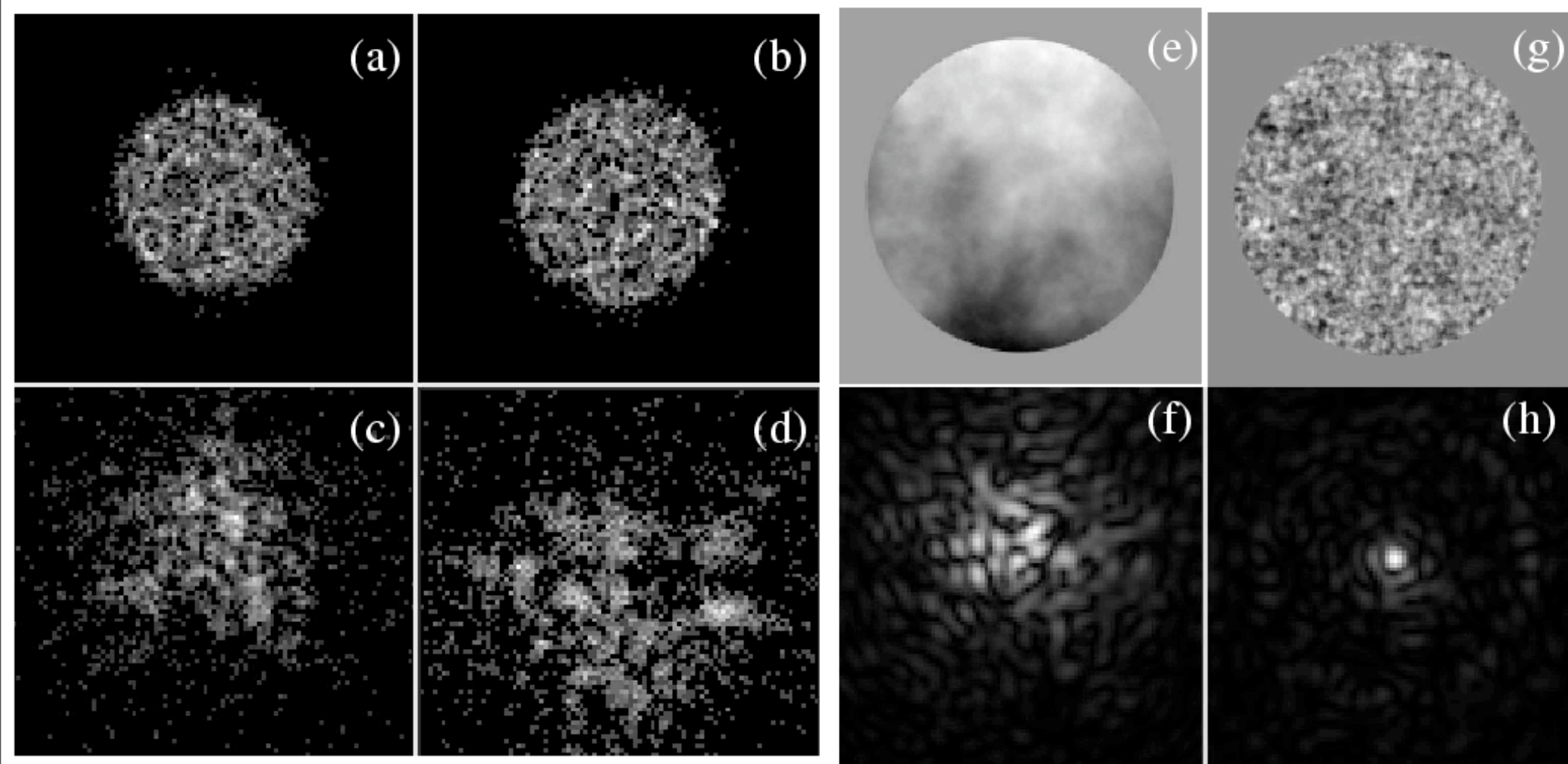
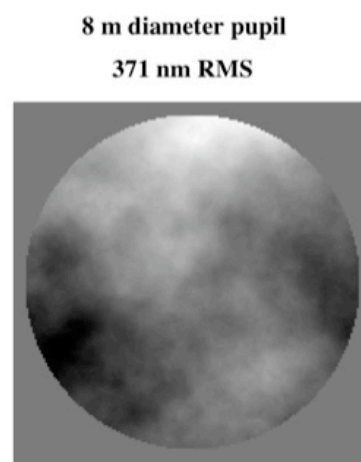
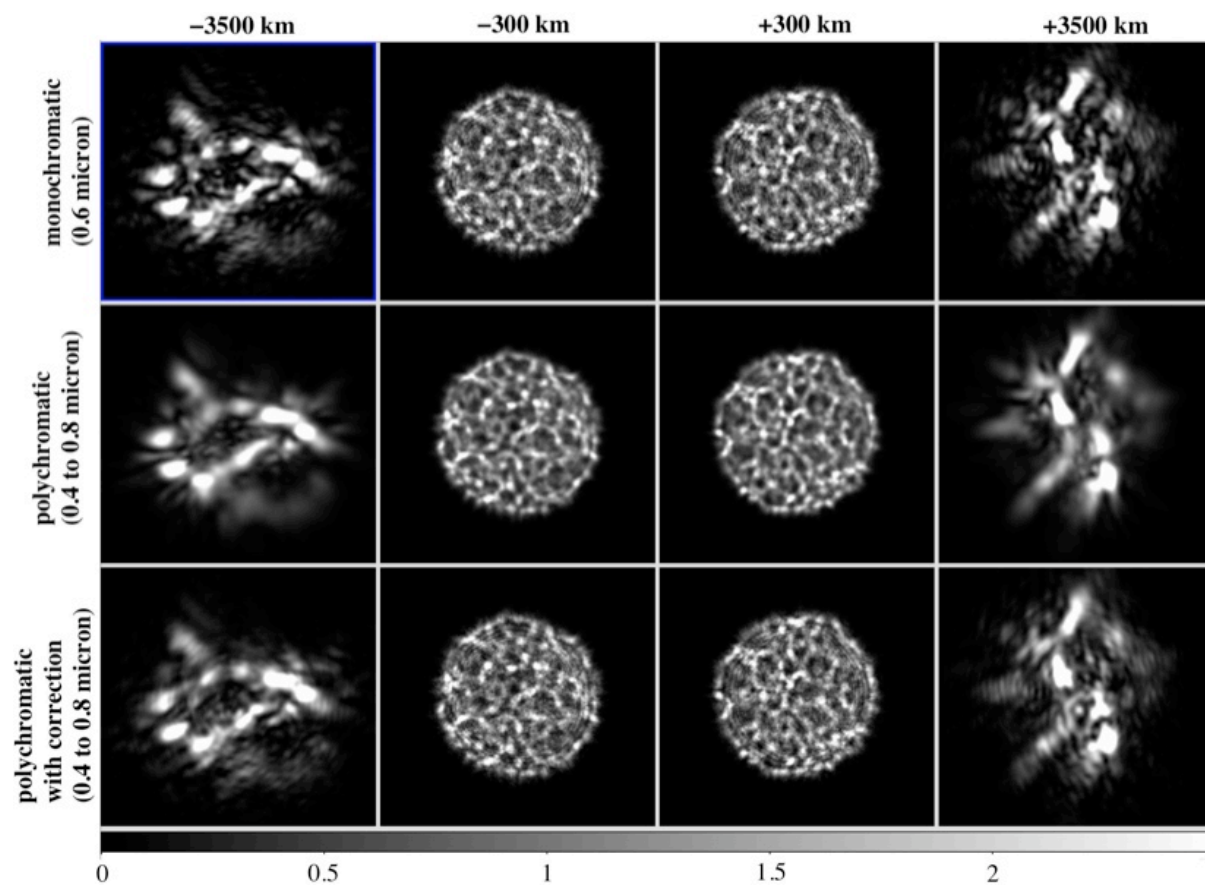
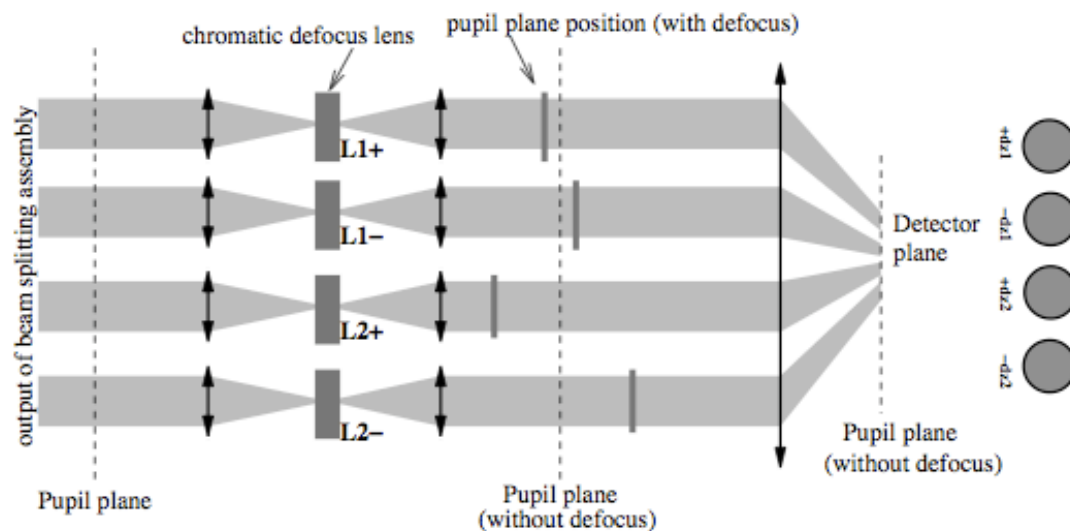
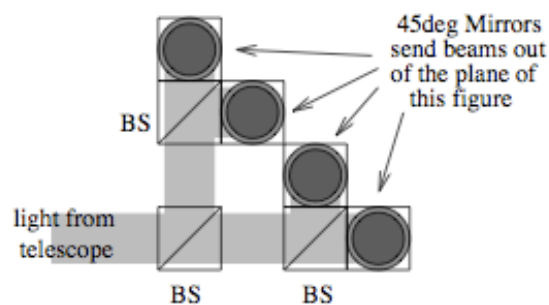


Fig. 9.— Wavefront reconstruction using the algorithm shown in fig. 8. Four noisy defocused pupil images (images (a), (b), (c) and (d)) are acquired to transform the pupil phase aberrations (e) into intensity signals. The input pupil phase is 609 nm RMS, yielding the PSF (f) before correction. After correction, the residual pupil phase aberration (g) is 34.4 nm RMS, allowing high Strehl ratio imaging (h). All images in this figure were obtained at $0.65\ \mu\text{m}$. The total number of photons available for wavefront sensing is $2e4$.

Beam splitting assembly produces 4 identical copies of beam from the telescope



$dI/I = 0$

105.8 nm

$dI/I = 0.2$

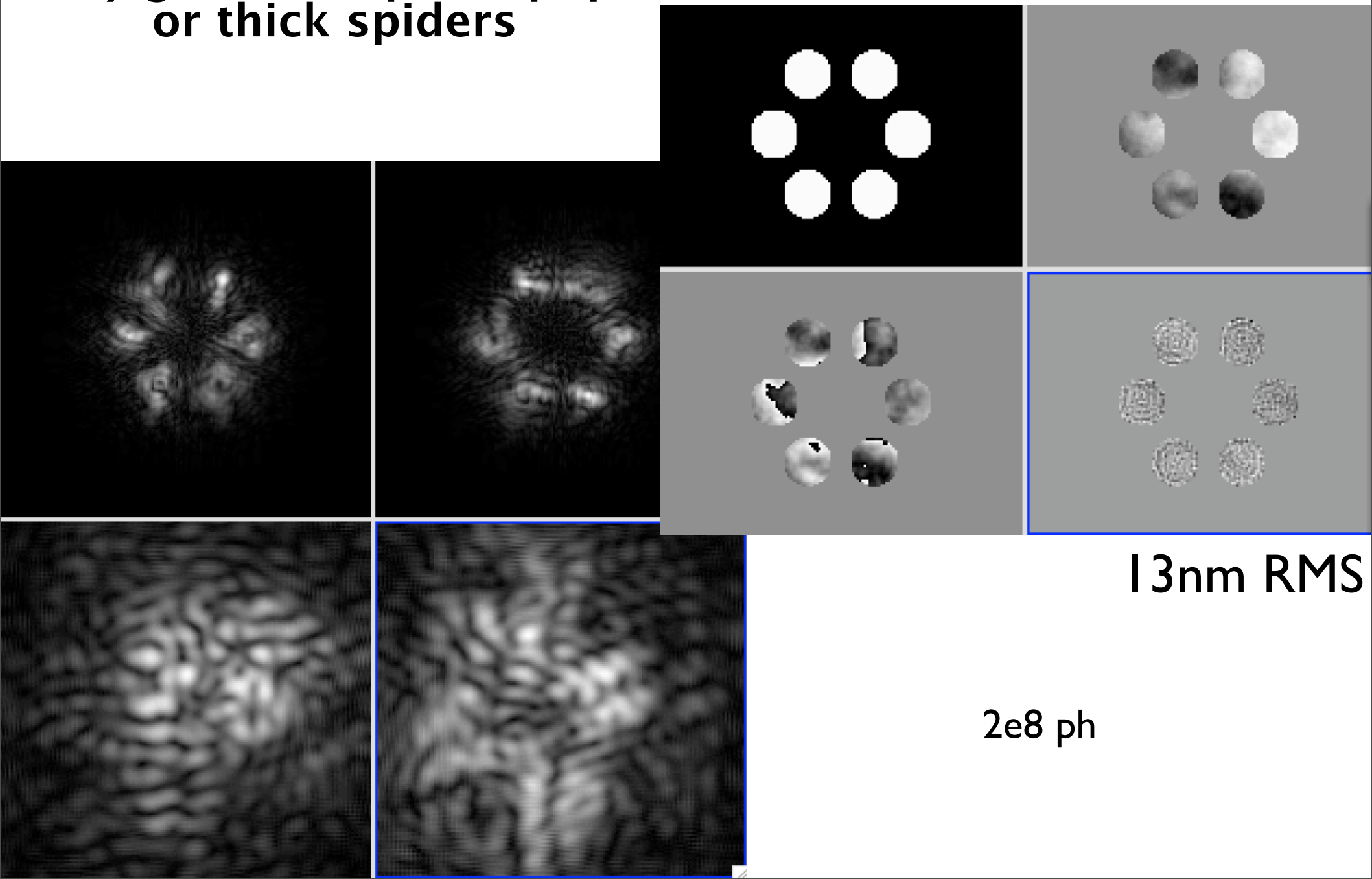
106.8 nm

$dI/I = 0.4$

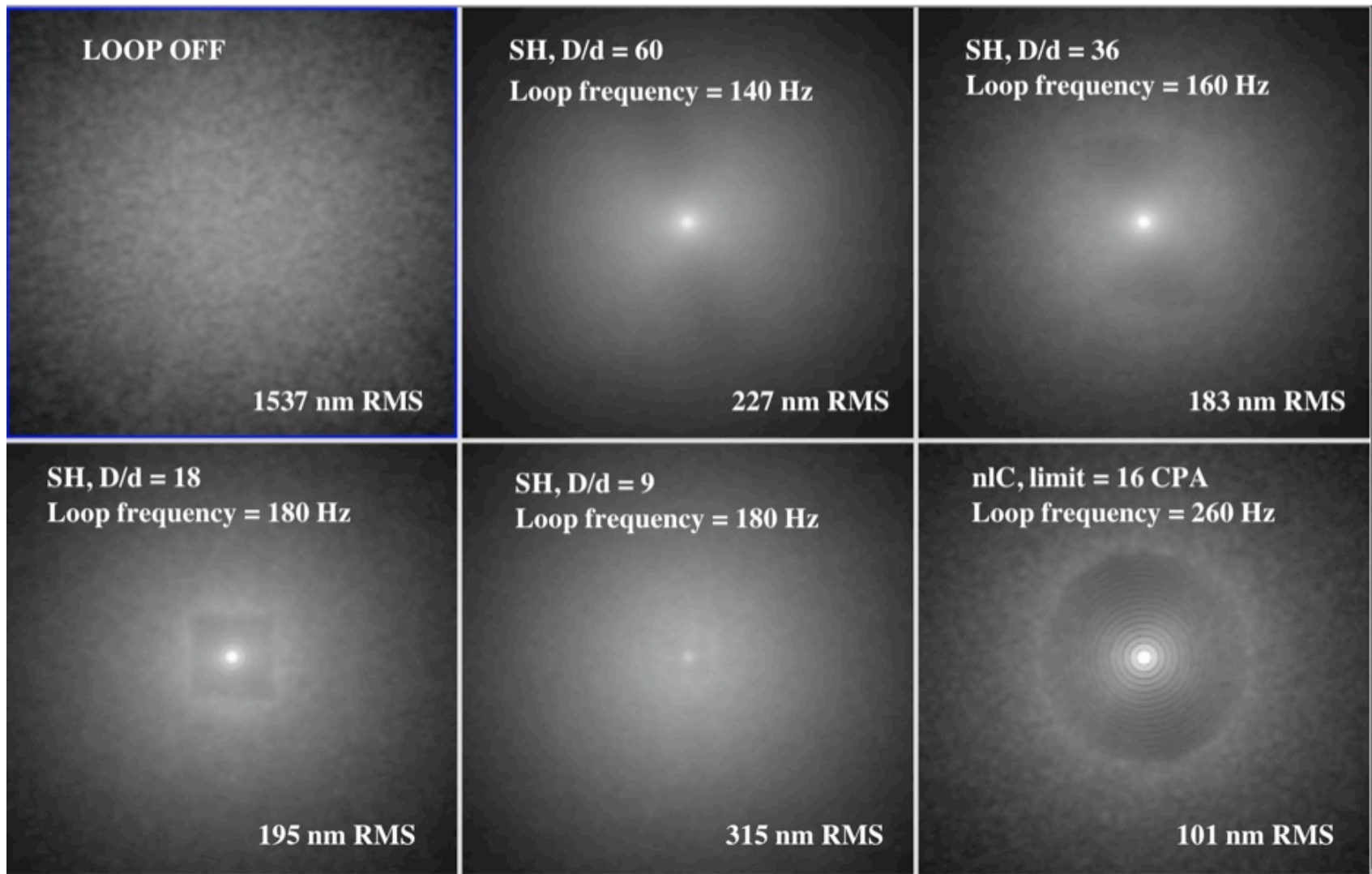
107.6 nm

Polychromatic nlCWFS with
monochromatic wavefront
reconstruction algorithm

Very good for Sparse pupil
or thick spiders



$m \sim 13$



WFS	Loop frequ	RMS	SR @ 0.85 μ	SR @ 1.6 μ
nlCurv	260 Hz	101 nm	57%	85%
SH - D/9	180 Hz	315 nm	~4%	22%
SH - D/18	180 Hz	195 nm	~13%	56%
SH - D/36	160 Hz	183 nm	~16%	60%
SH - D/60	140 Hz	227 nm	~6%	45%

Example of loss due to temporal coherence.
 Note how choosing longer sensing wavelength helps by
 increasing wavefront coherence (even though phase signal gets
 smaller !!!)

Closed loop
 simulations

WFS:
 non-linear
 phase retrieval
 on curvature
 wavefront sensor

Same behaviour
 would be obtained
 with fixed pyramid

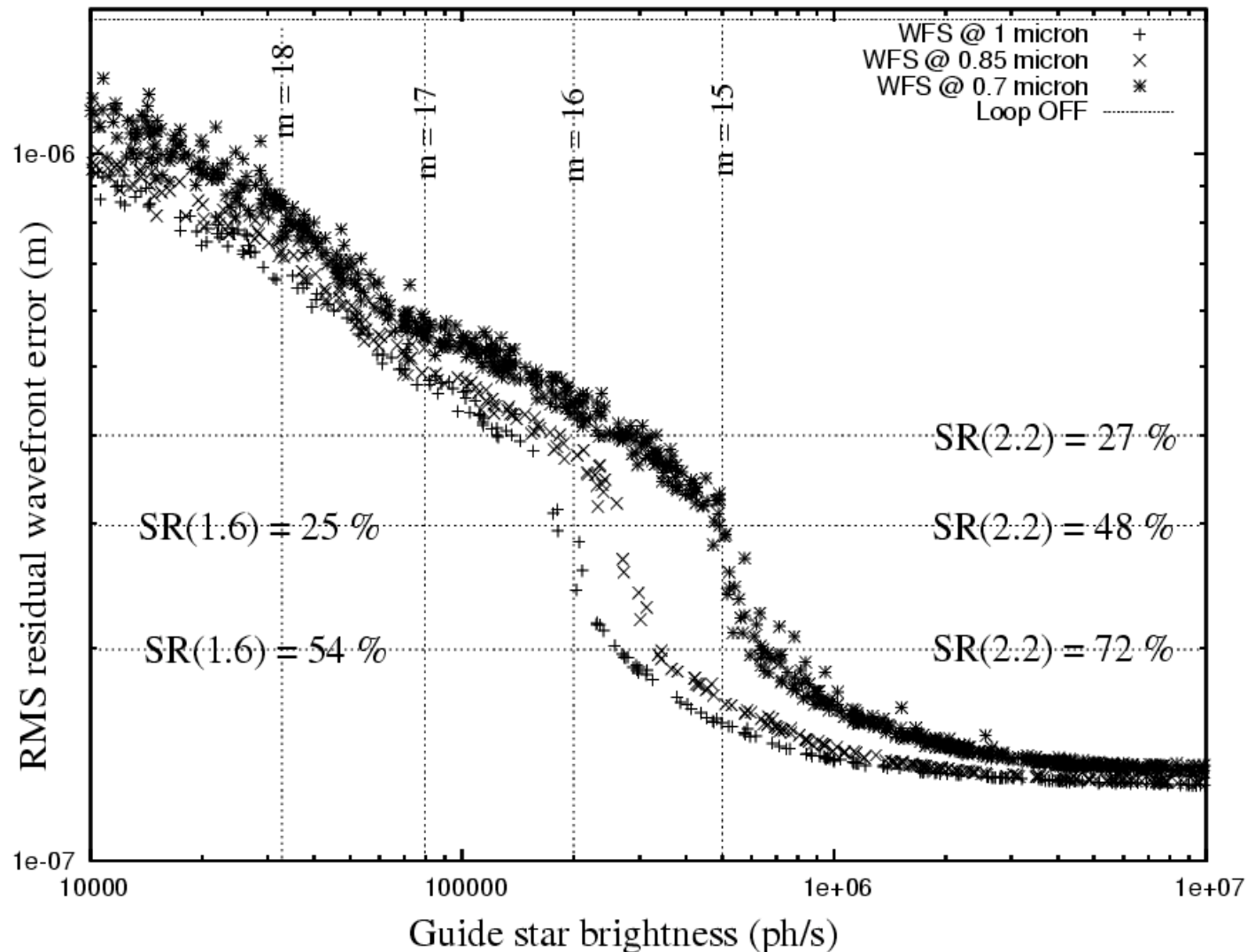


Fig. 11.— Simulated performance of a non-linear Dual stroke Curvature as a function of sensing wavelength (0.7, 0.85 and 1.0 μm) and guide star brightness. The stellar magnitudes given in this figure assume a 20% efficiency in a 0.5 μm wide band. See text for details.

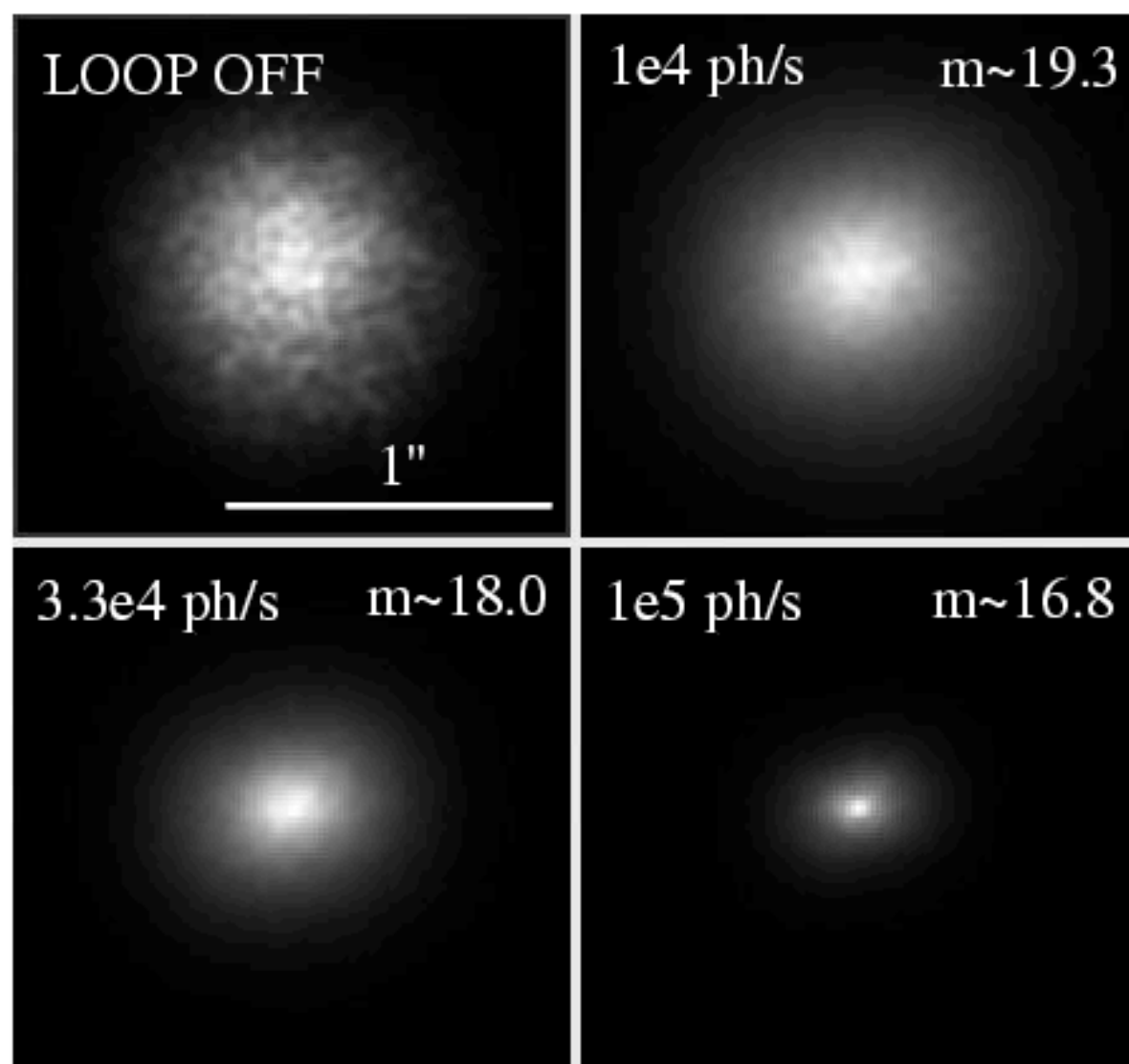
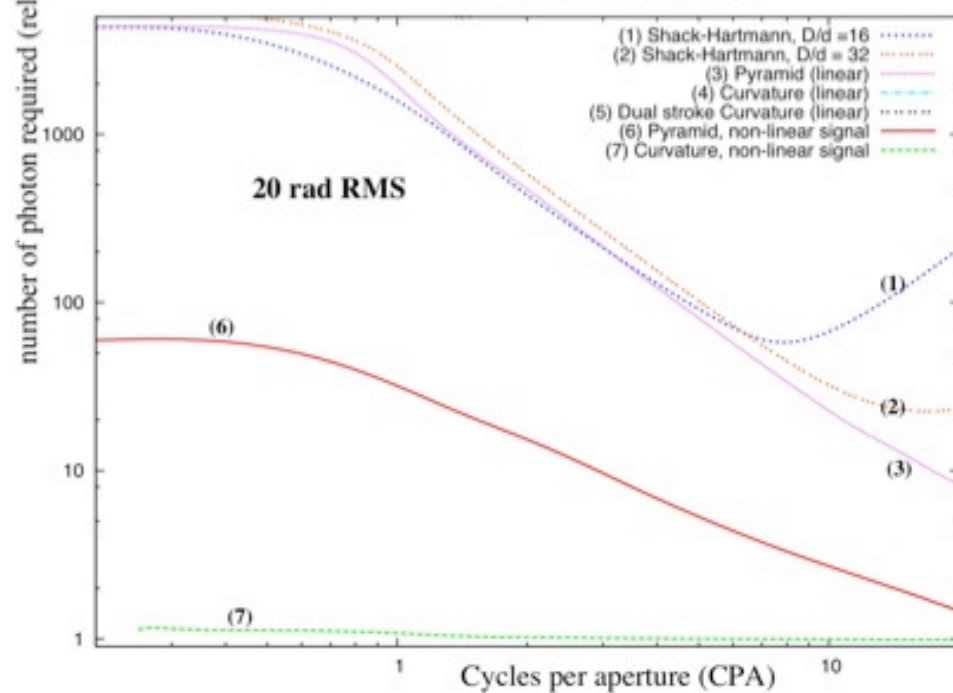
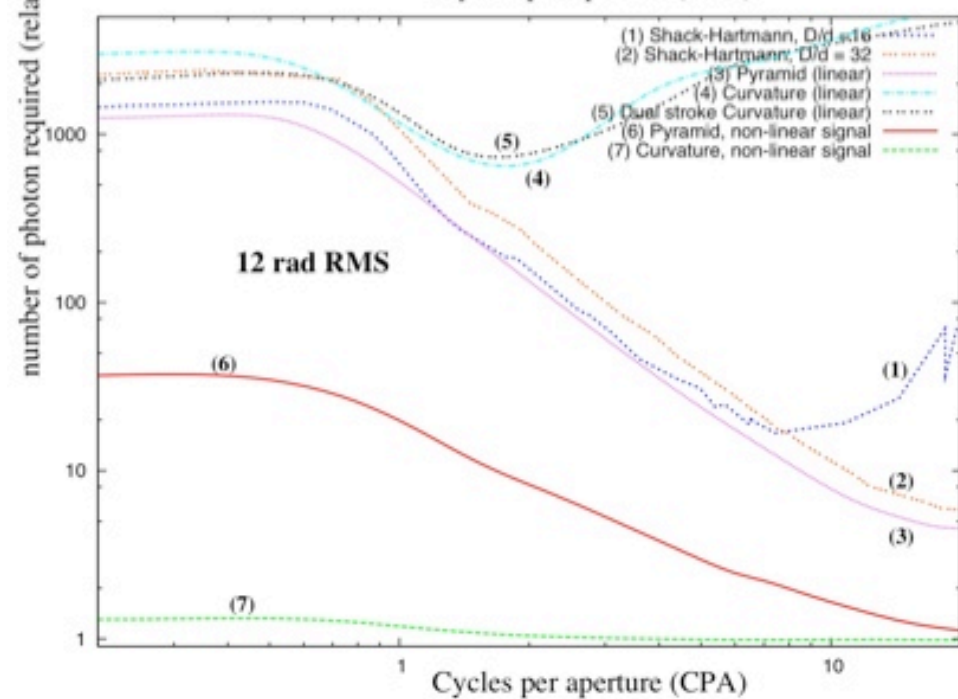
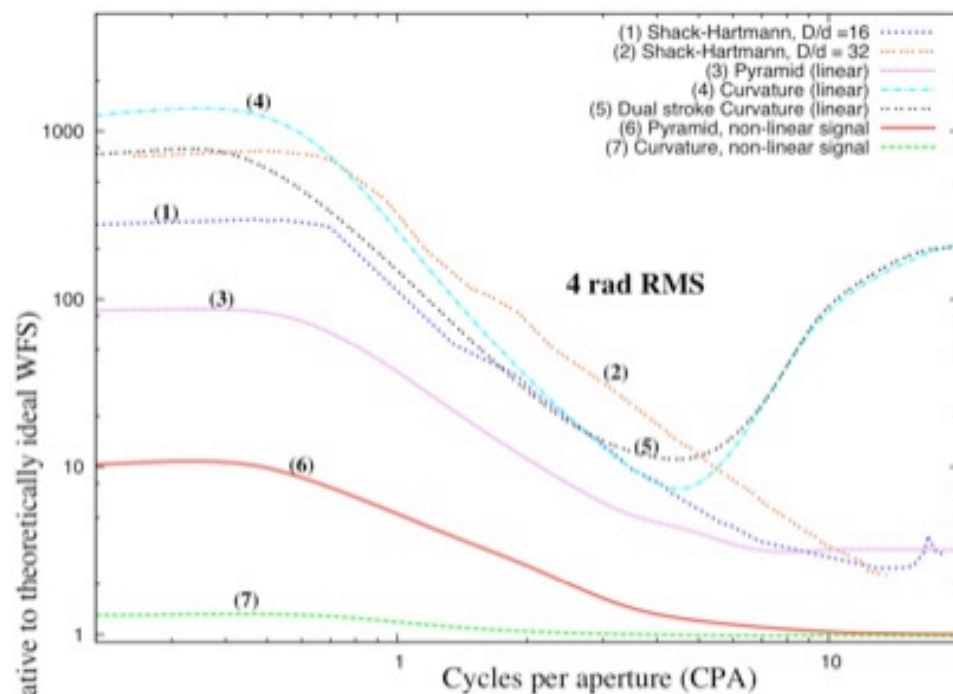
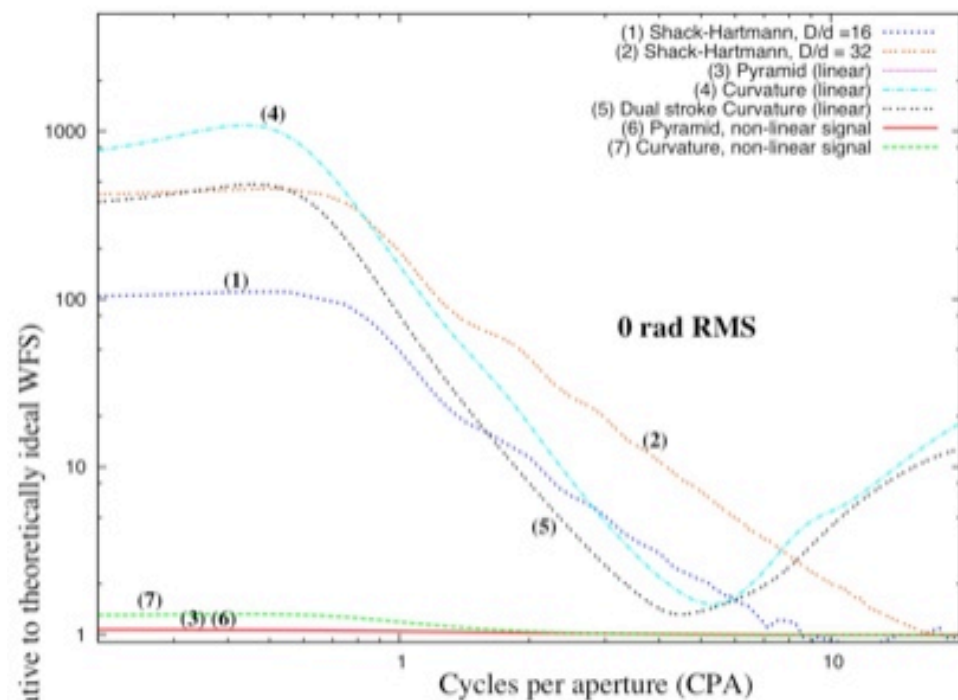


Fig. 12.— Simulated long exposure $1.6\ \mu\text{m}$ PSFs obtained with a non-linear Dual stroke Curvature-based AO system. The sensing wavelength was $0.85\ \mu\text{m}$ for this simulation.



Focal plane WFS

How to **optimally** measure speckle field complex amplitude ?

Use upstream DM to introduce phase diversity.

Conventional phase diversity: focus

With DM: **freedom to tune the diversity to the problem**

Measure speckle field with no previous knowledge:

- take one frame – this gives a noisy measure of the speckle field amplitude, but not phase
- compute 2 DM shapes which will add known speckles on top of existing speckles. These 2 “additive” speckle field have same amplitude as existing speckles, and the phase offset between the 2 additive speckle fields is $\pi/2$
- > for each point in the focal plane, 3 intensities –> single solution for phase & amplitude of speckle field

Speckles vs. planet

Spectra differential imaging (SDI)

Optimized for methane-bearing giant planets

Will only detect planets with a given spectral feature

Polarization differential imaging (PDI)

Degree of polarization may be low (few %)

Only works on reflected light

Angular differential imaging (ADI)

Performs well if static speckles are strong

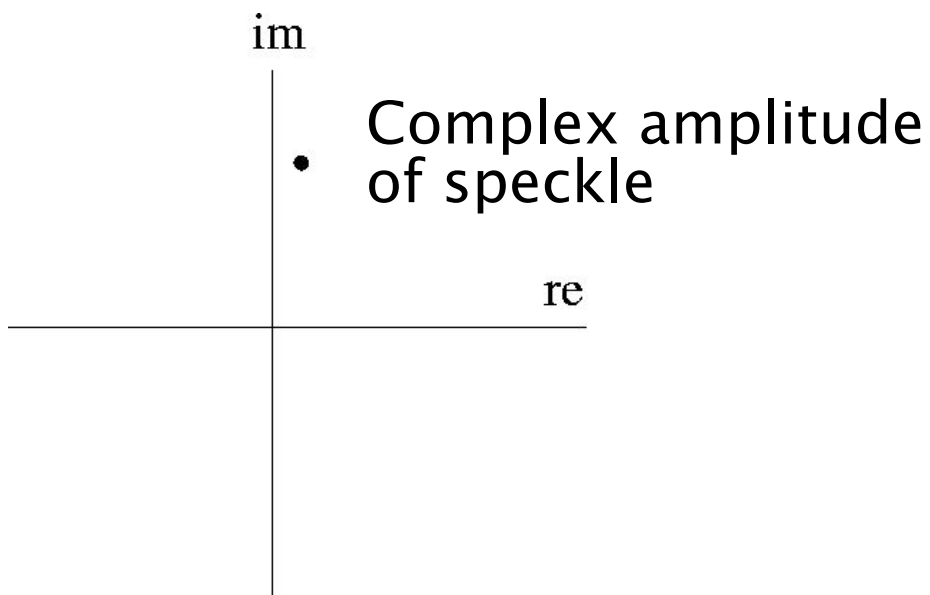
Does not work well at small angular separations

Coherent differential imaging (CDI)

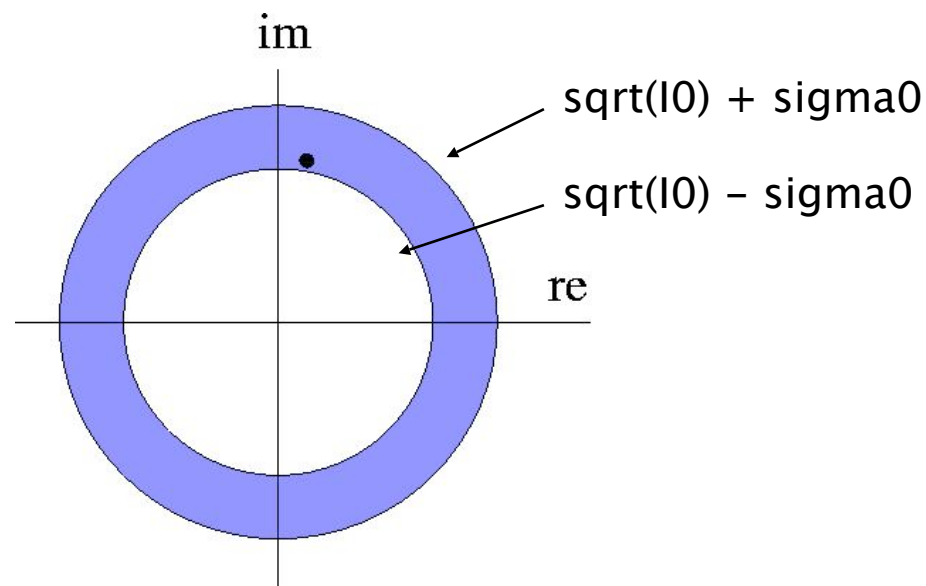
Use DM to introduce a known variation in the WF to modulate speckle intensity

Can reach photon noise limit if system is very well calibrated and CDI is performed quickly (or simultaneously)

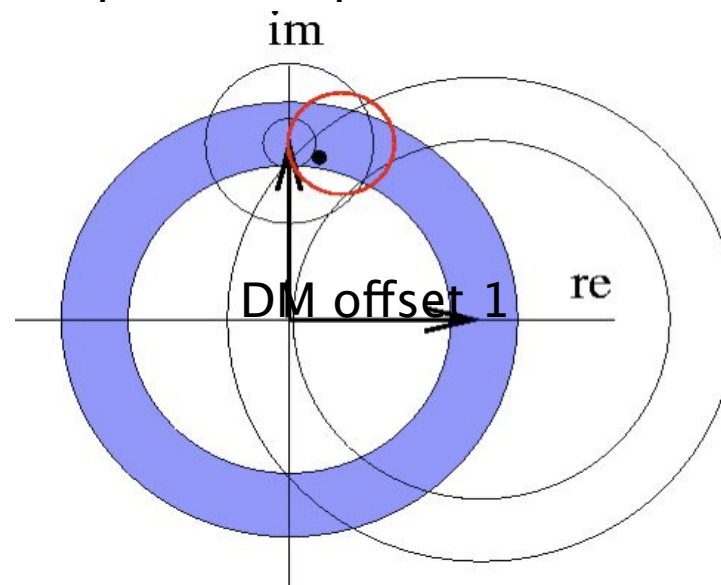
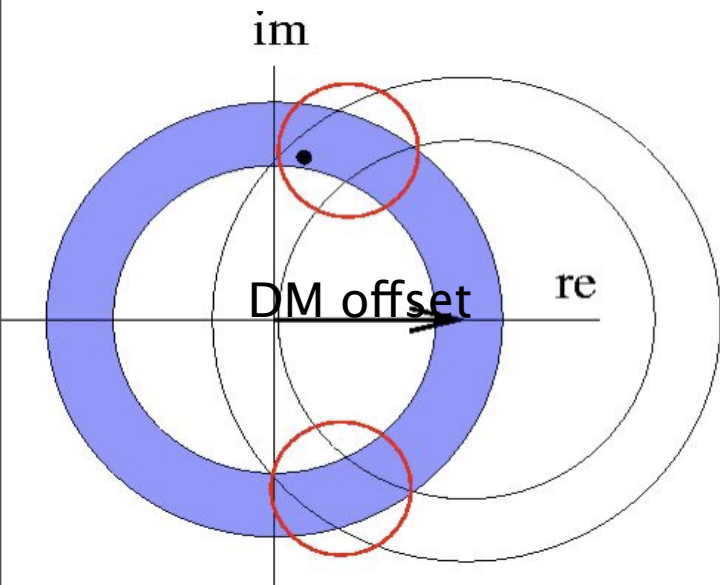
Initial problem



Take a frame $\rightarrow$ measured
speckle intensity = I_0



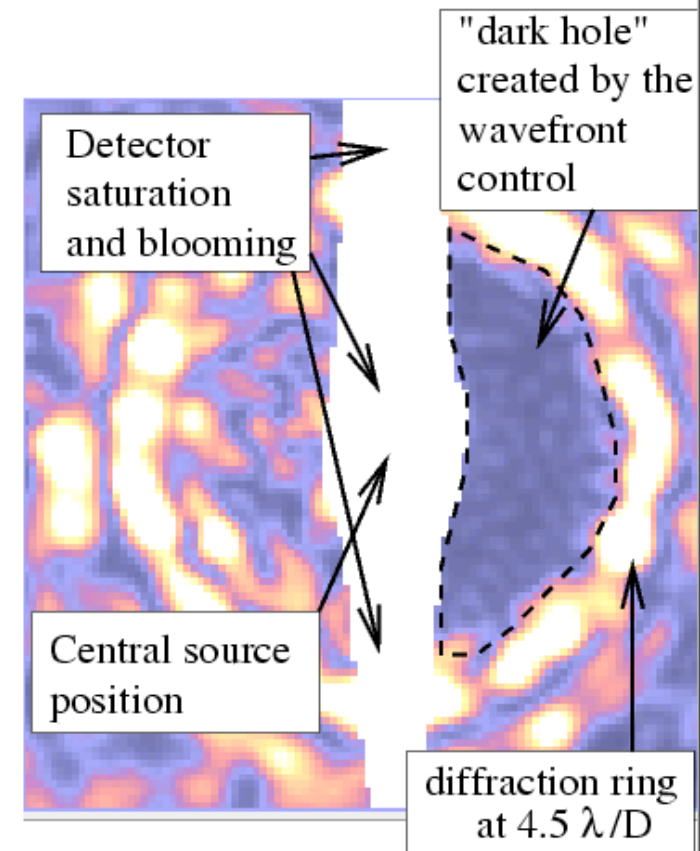
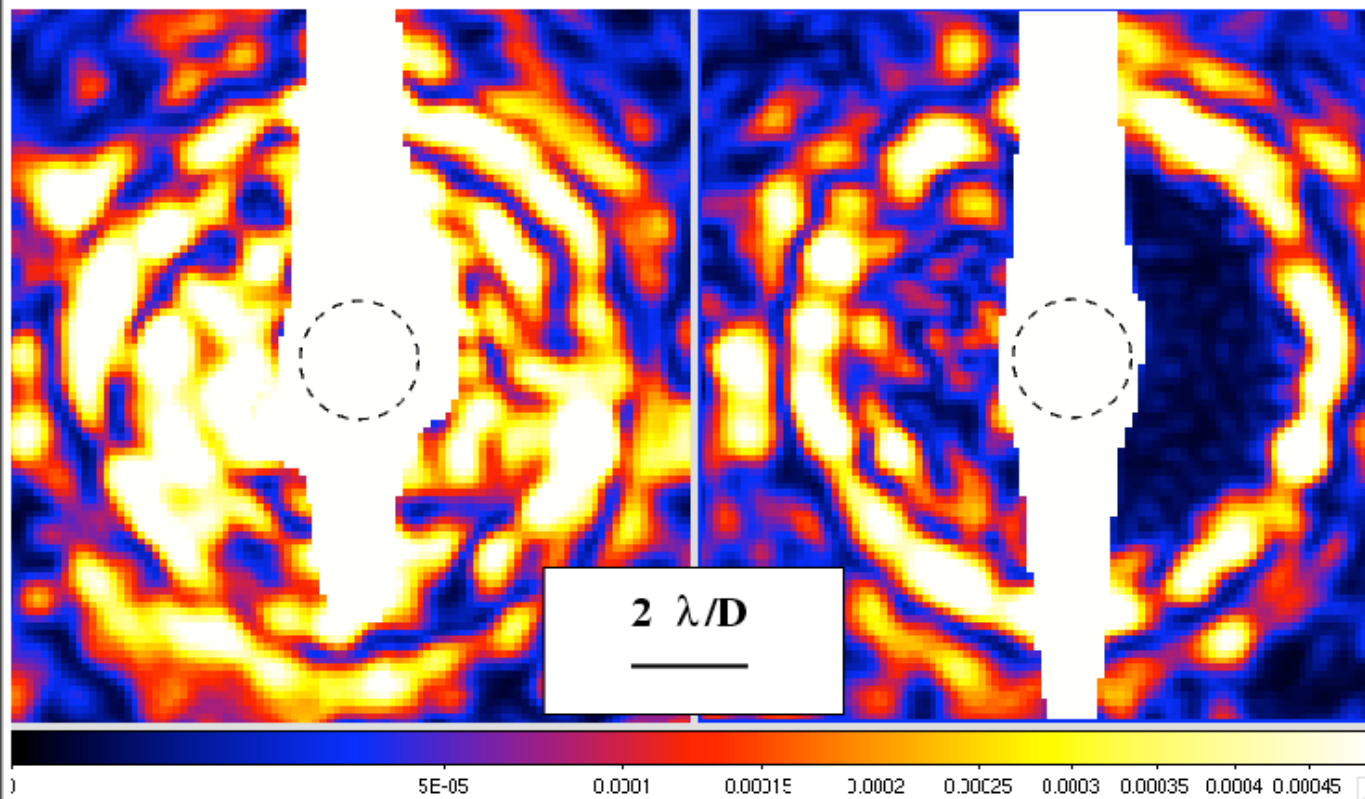
DM offset chosen to be $\sim$ equal to speckle amplitude



Lab results with PIAA coronagraph + FPAO with 32x32 MEMs DM

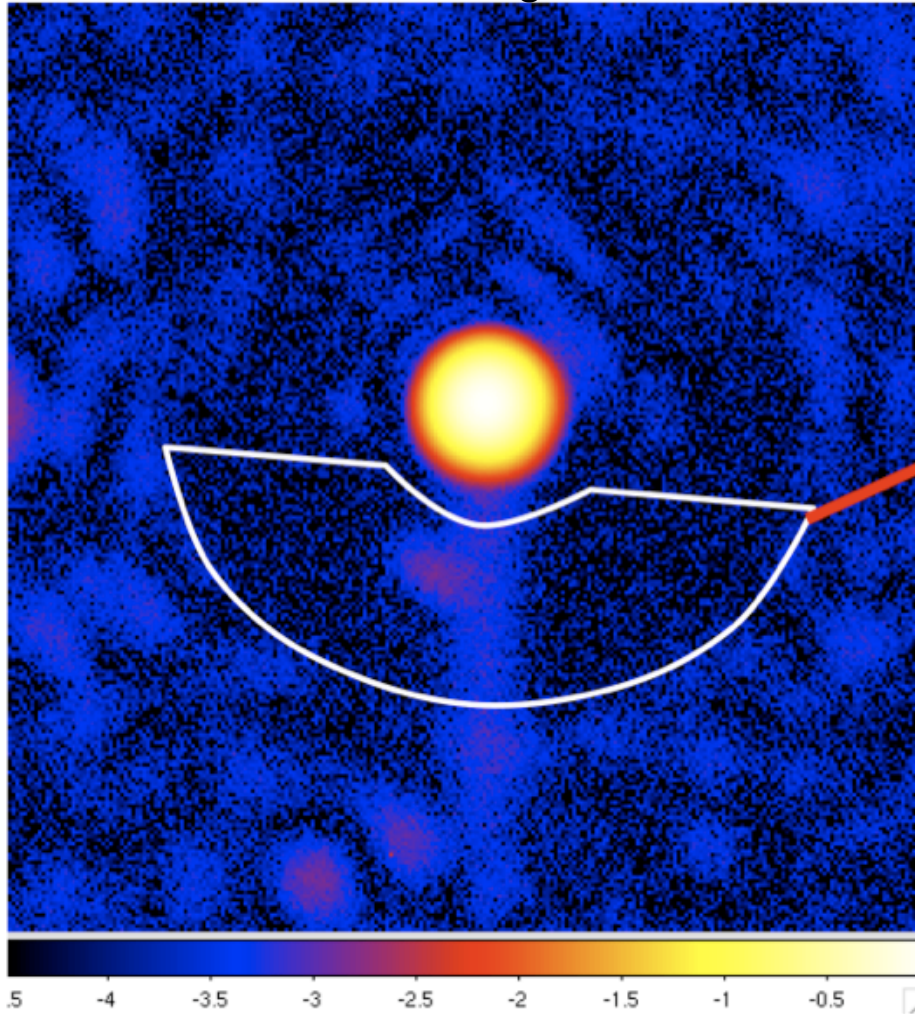
FPAO loop OFF

FPAO loop ON

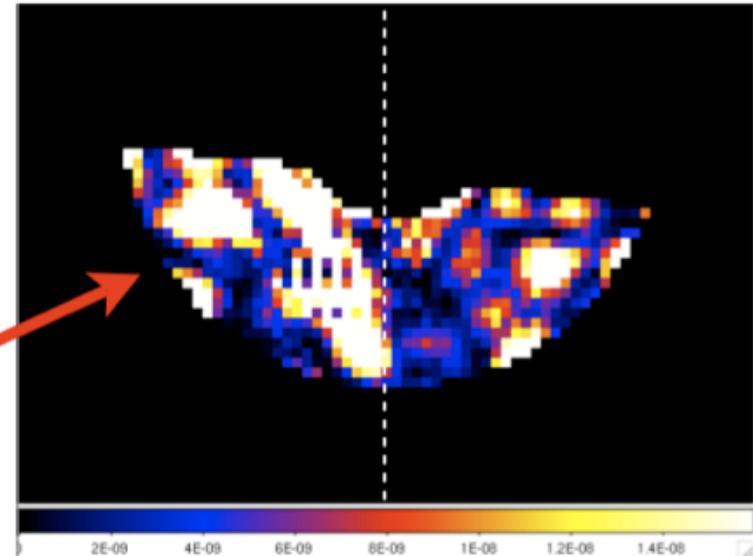


Recent lab results demonstrate PIAA coronagraph + Focal plane AO + coherent differential imaging

Raw image



Coherent starlight



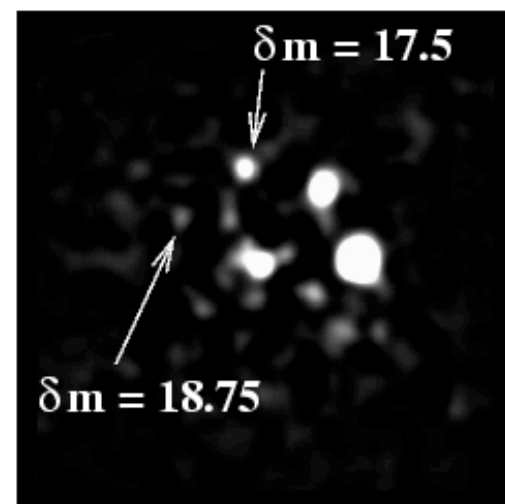
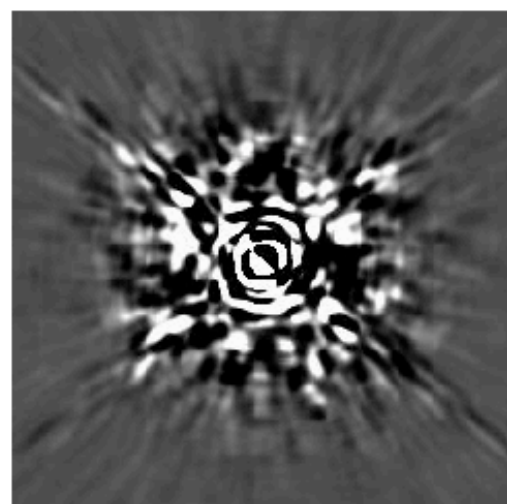
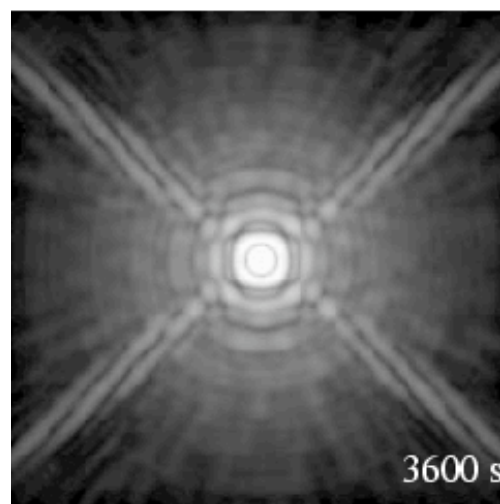
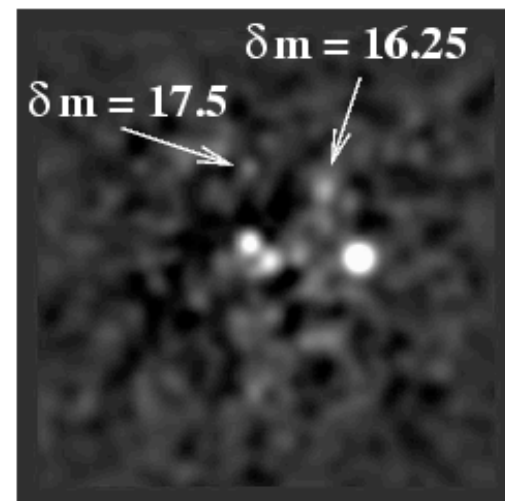
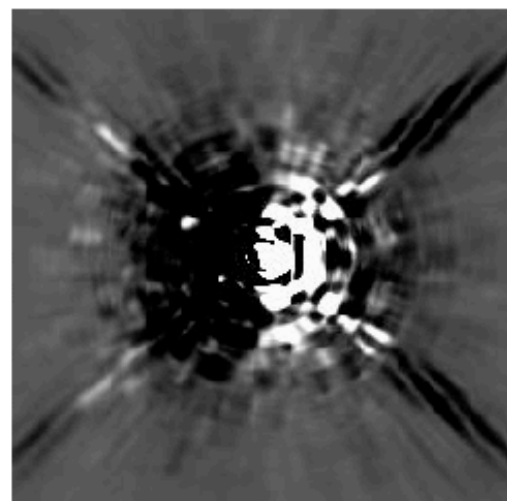
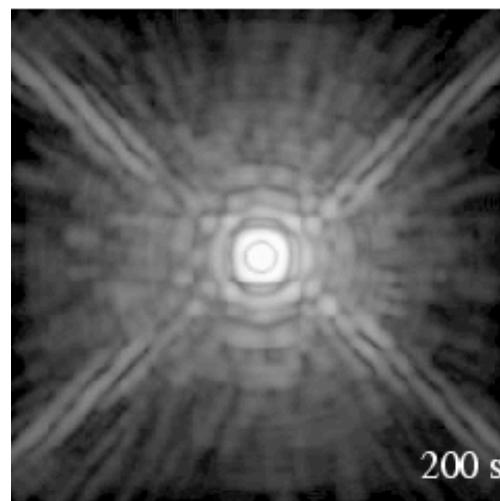
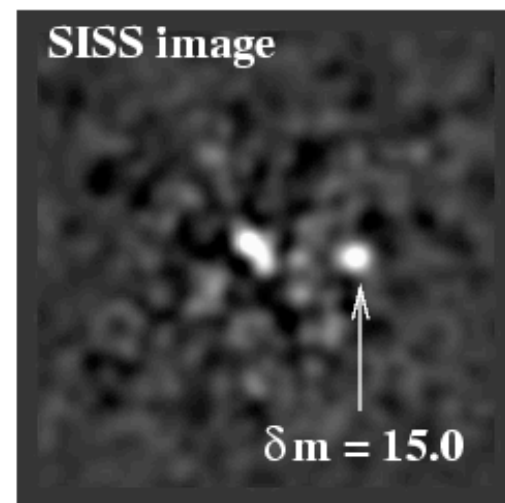
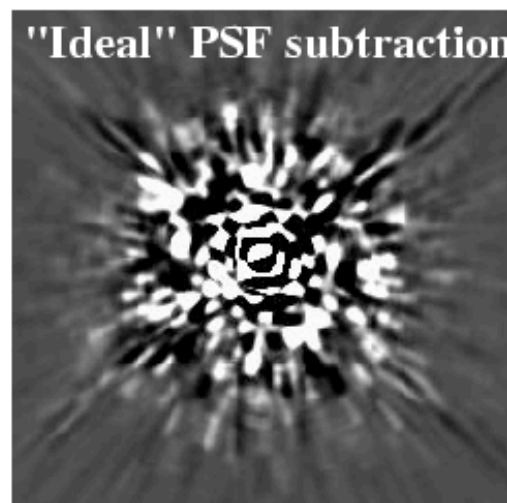
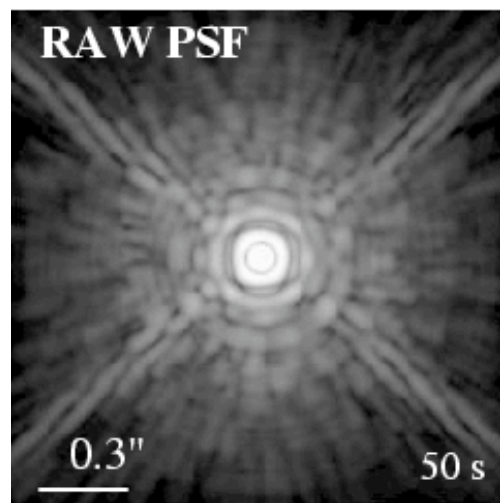
Average contrast in right half of the science field shown above (excludes the ghost on the left) = $7e-9$

Contrast achieved in 1.6 to 4.5 I/D zone:

$1.5e-7$ incoherent halo ghost (equivalent to exozodi)

$7e-9$ coherent starlight speckles (turbulence, vibrations)

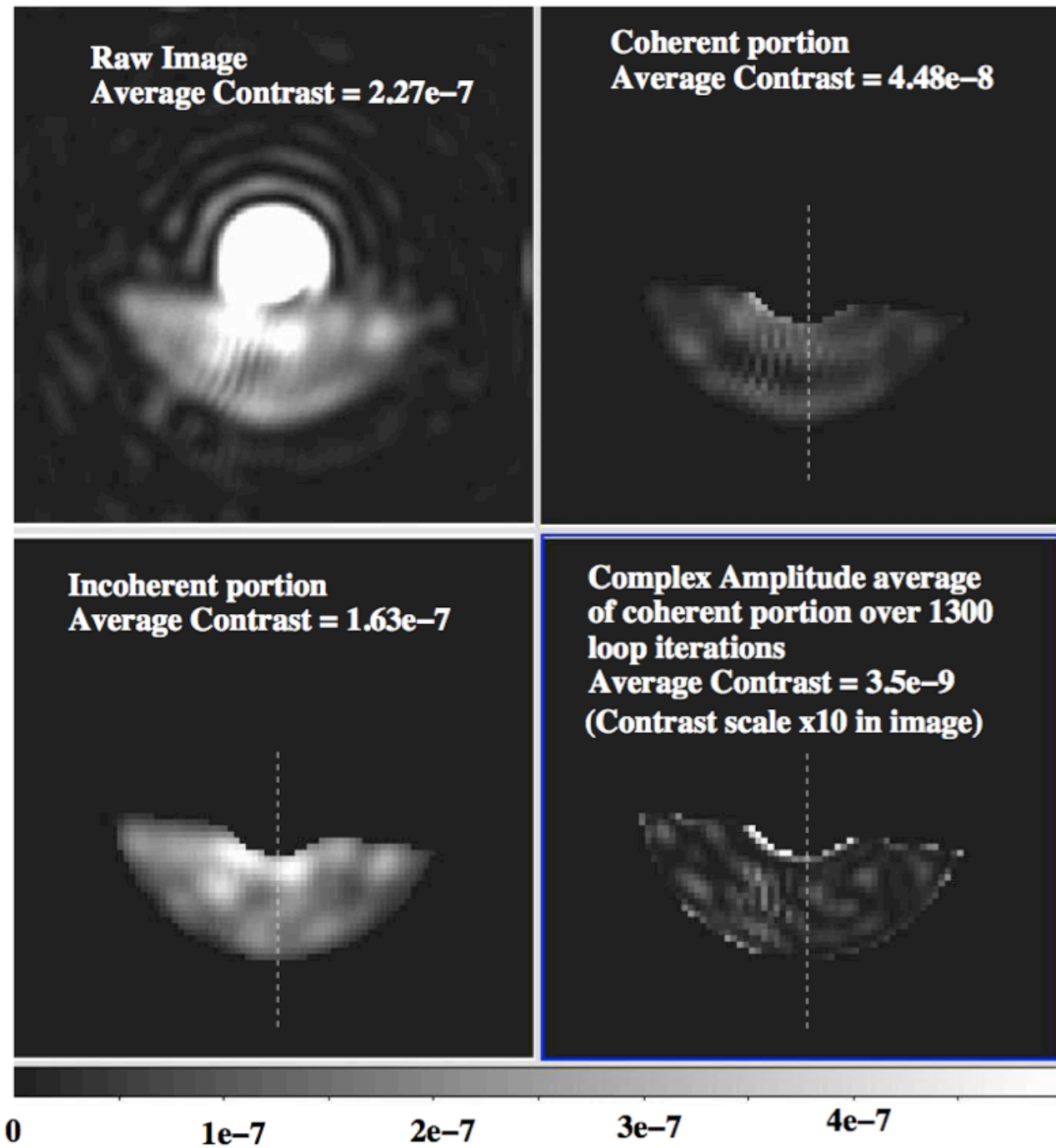
Speckle calibration with active coherent modulation



Coherent detection
works in the lab
alongside FPAO

Extremely powerful for
ExAO:

- Optically simple
- Non NCPE
- on-the fly diagnostics
- CDI post-processing



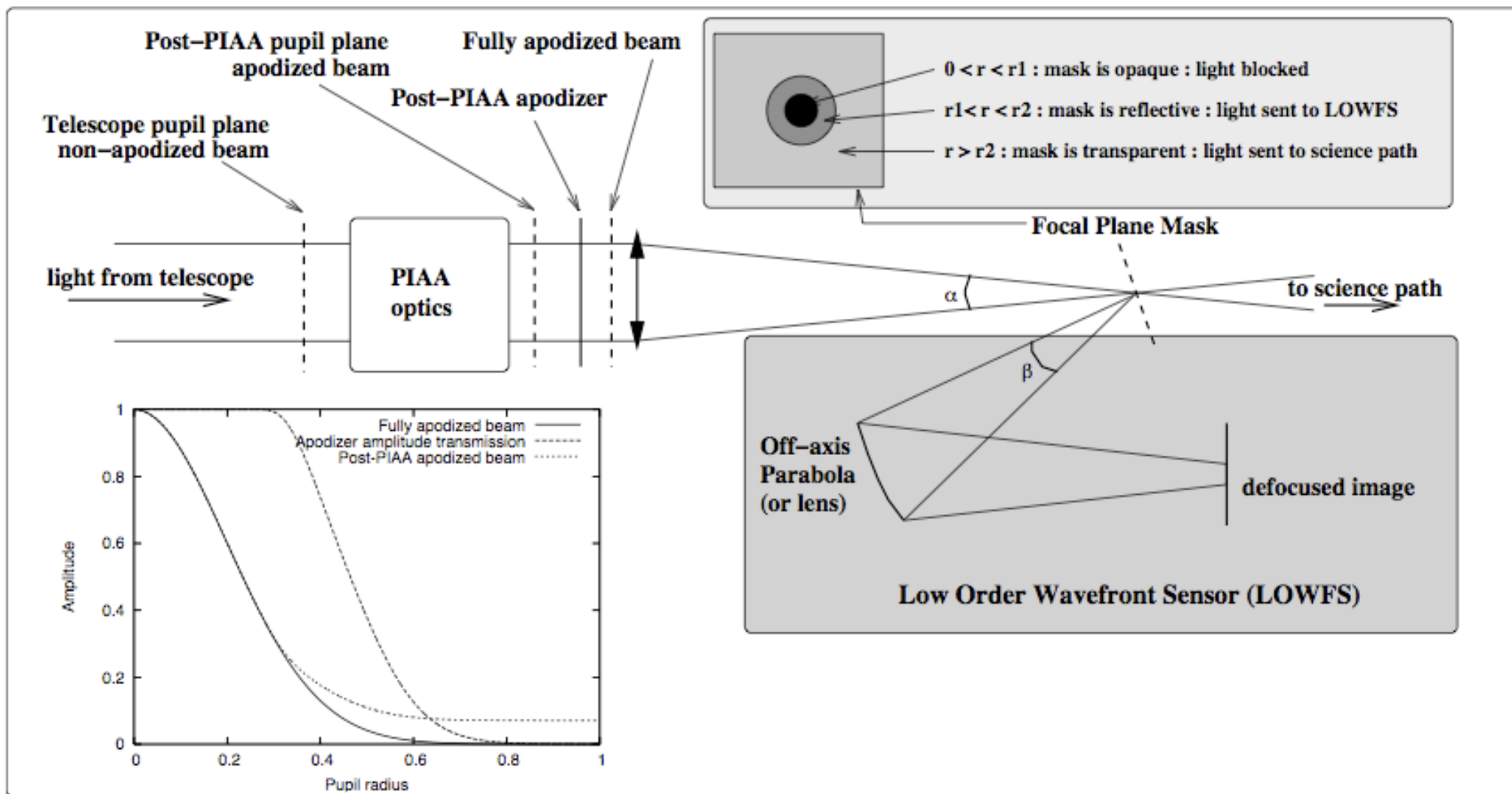
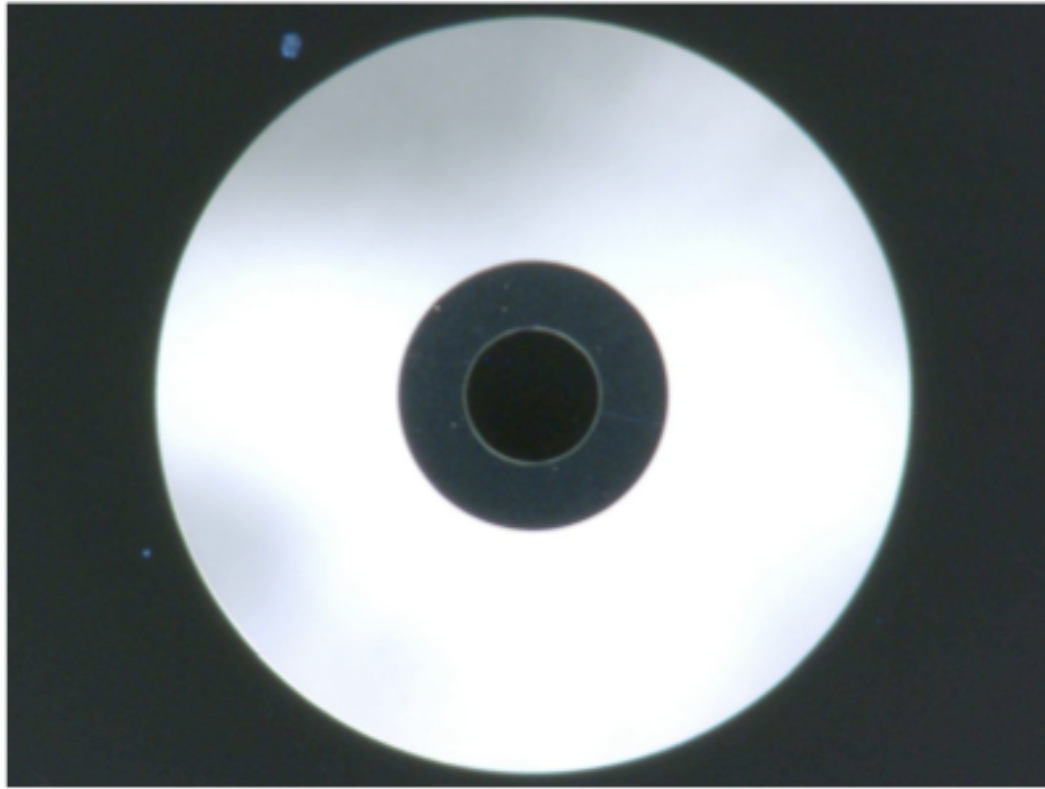


Fig. 1.— Optical layout of a coronagraphic low order wavefront sensor system, shown here with a PIAA coronagraph. See text for details.

Guyon, Matsuo, Angel, 2008 - in press

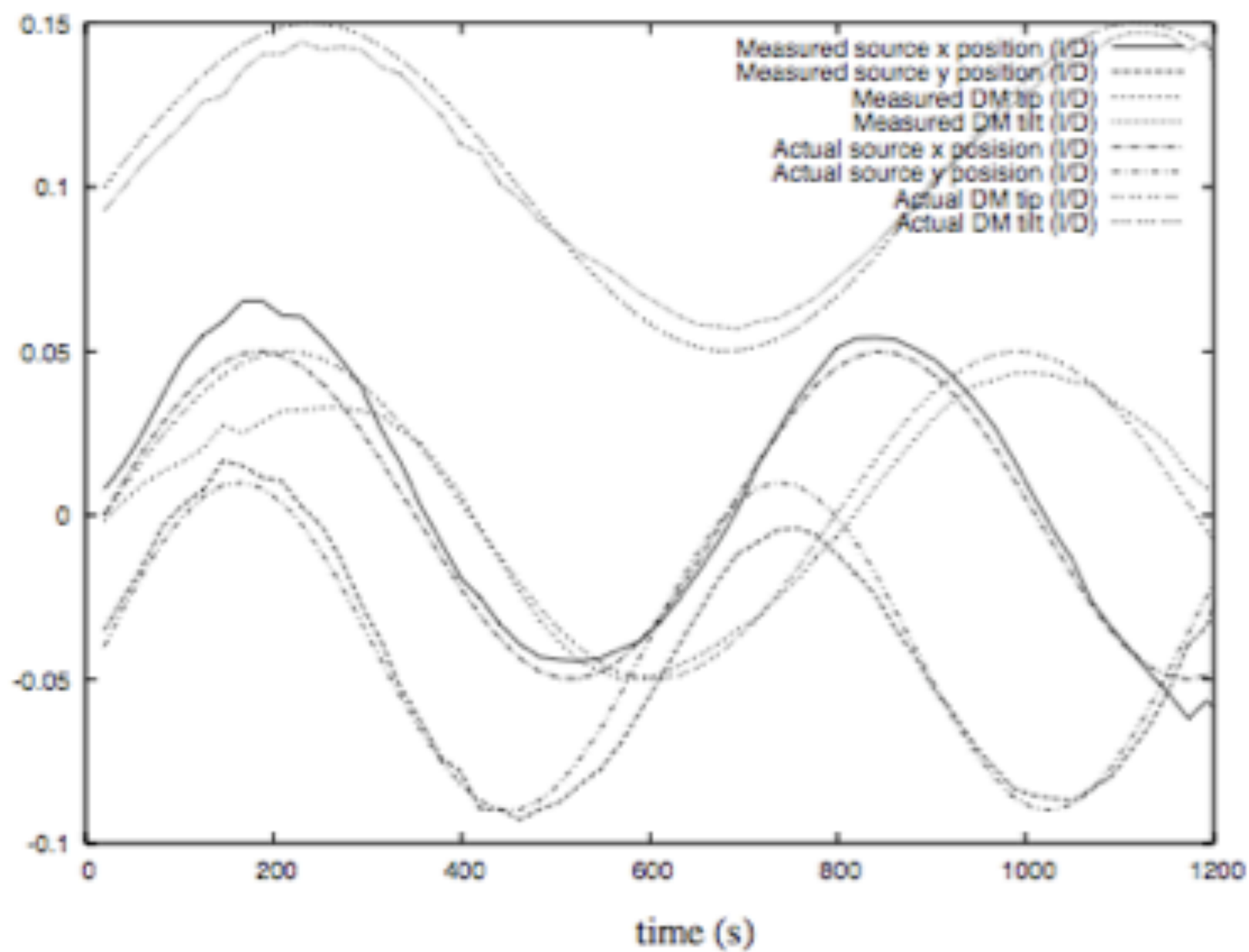
Can also be applied to phase mask type coronagraphs (Matsuo & Guyon, in preparation)



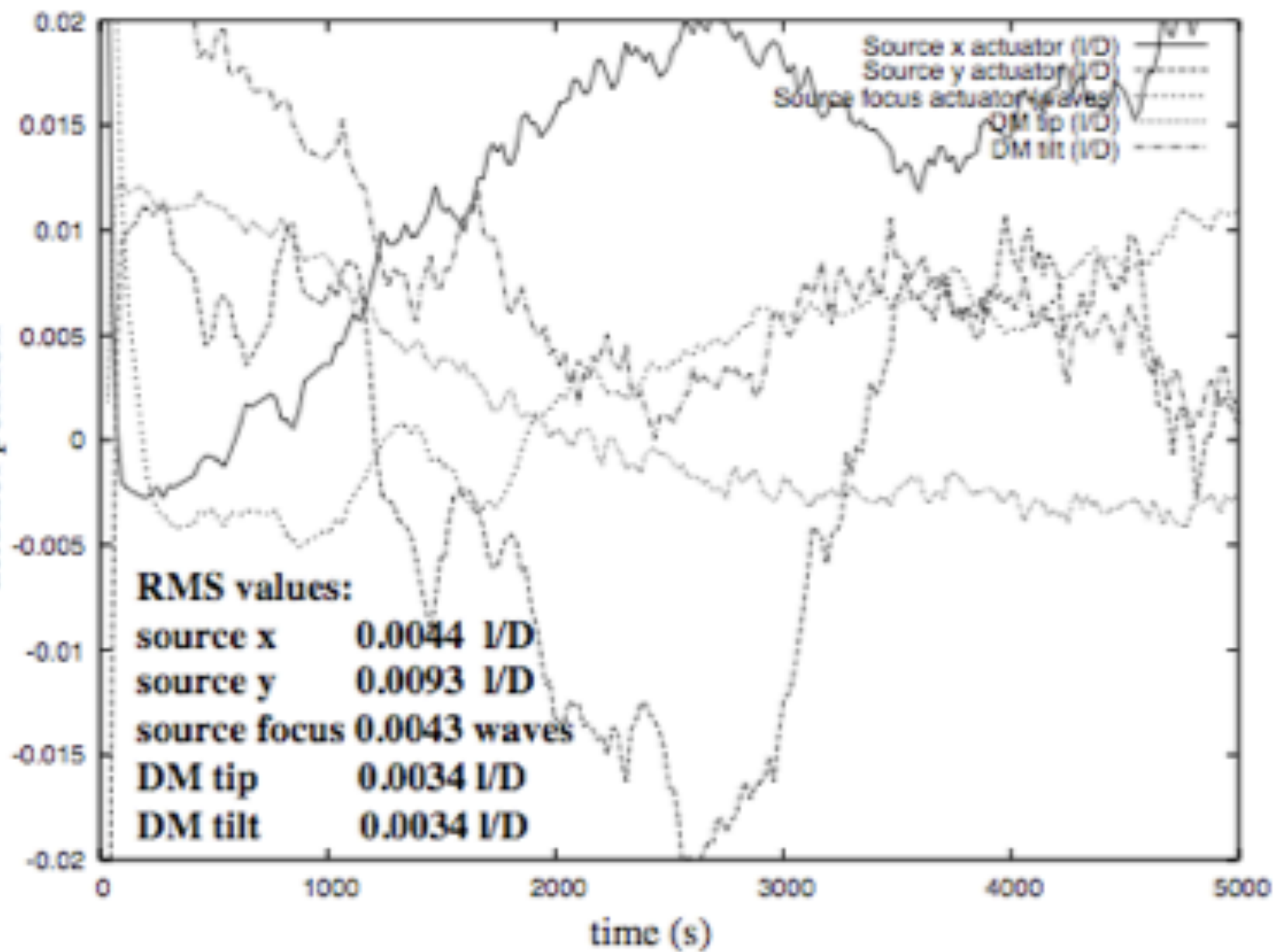
Why a central dark spot?

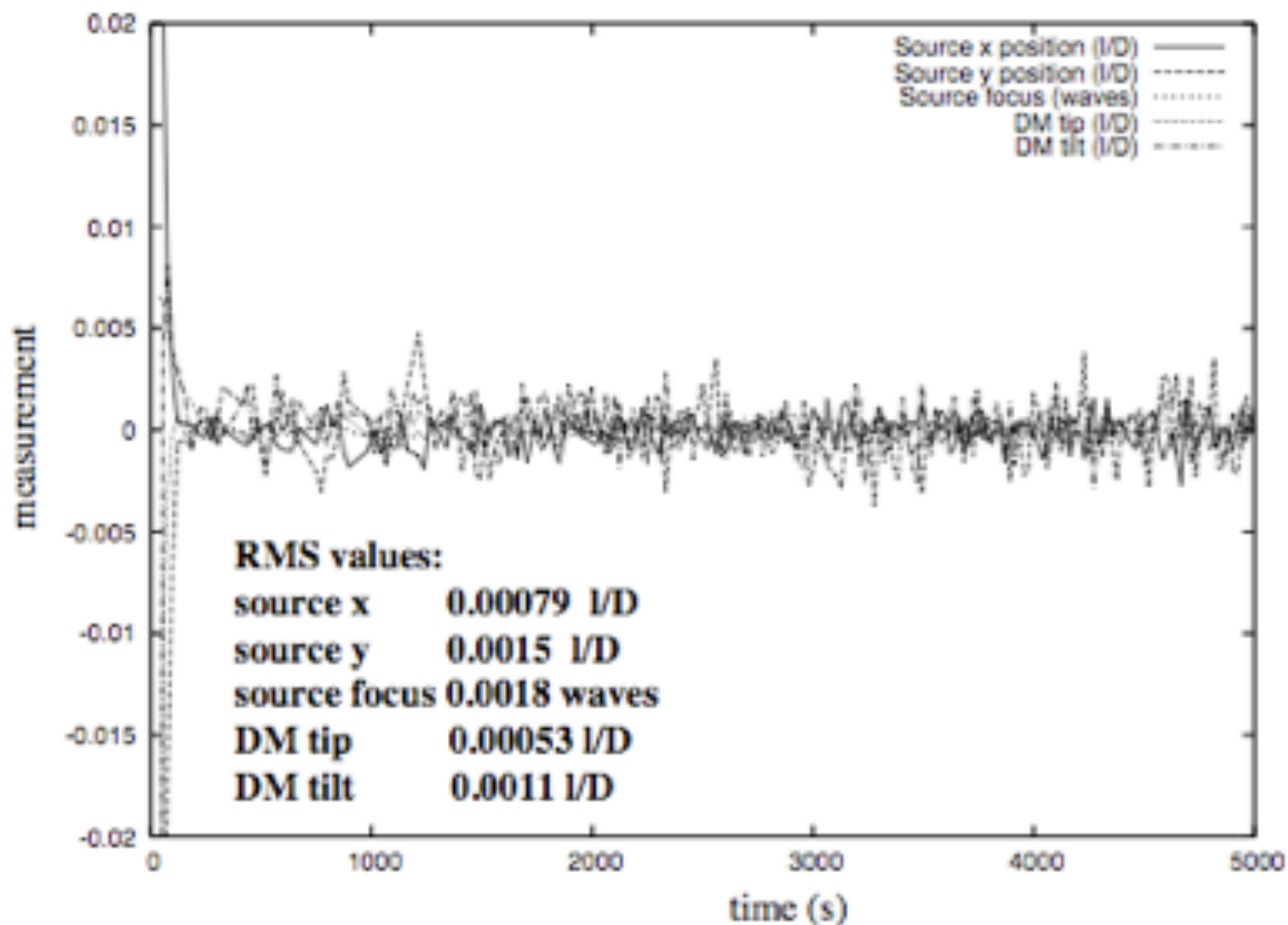
- (1) Signal amplification
- (2) Accurate reference

Fig. 9.— CLOWFS focal plane mask used in the PIAA coronagraph laboratory testbed at Subaru Telescope. The 100 micron radius mask center is opaque (low reflectivity), and is surrounded by a 100 micron wide highly reflective annulus. The science field, transmitting light to the science camera, extends from 200 micron to 550 micron radius.



actuator position



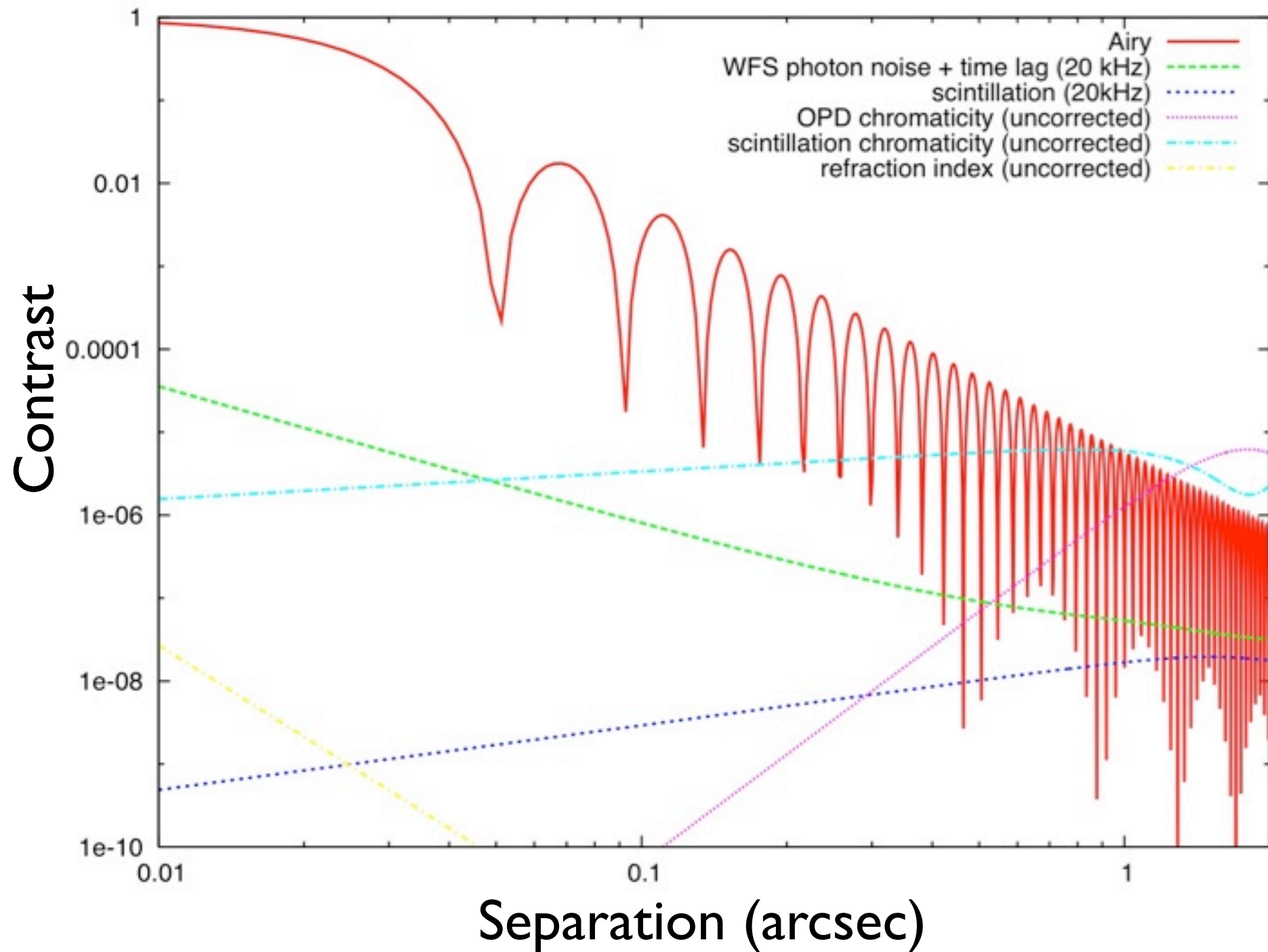


Can we image Earths with ground-based telescopes ?

Reflected light:

- Earth/Sun contrast $\sim 1\text{e-}9$
- SuperEarth $\sim 4\text{e-}9$
- Jupiter @ 1 AU: $2.5\text{e-}8$

8-m telescope



8m telescope, very good ExAO + slow near-IR correction

$mV = 5, mH = 5$

Contrast in H $\sim 1e-5 \sim 1e4$ ph/s/speckle (H band background $\sim 1/2$ of this)

with ~ 10 Hz residual speckle timescale

Photon noise from Halo = $1e-7 \times 1/\sqrt{t(s)}$

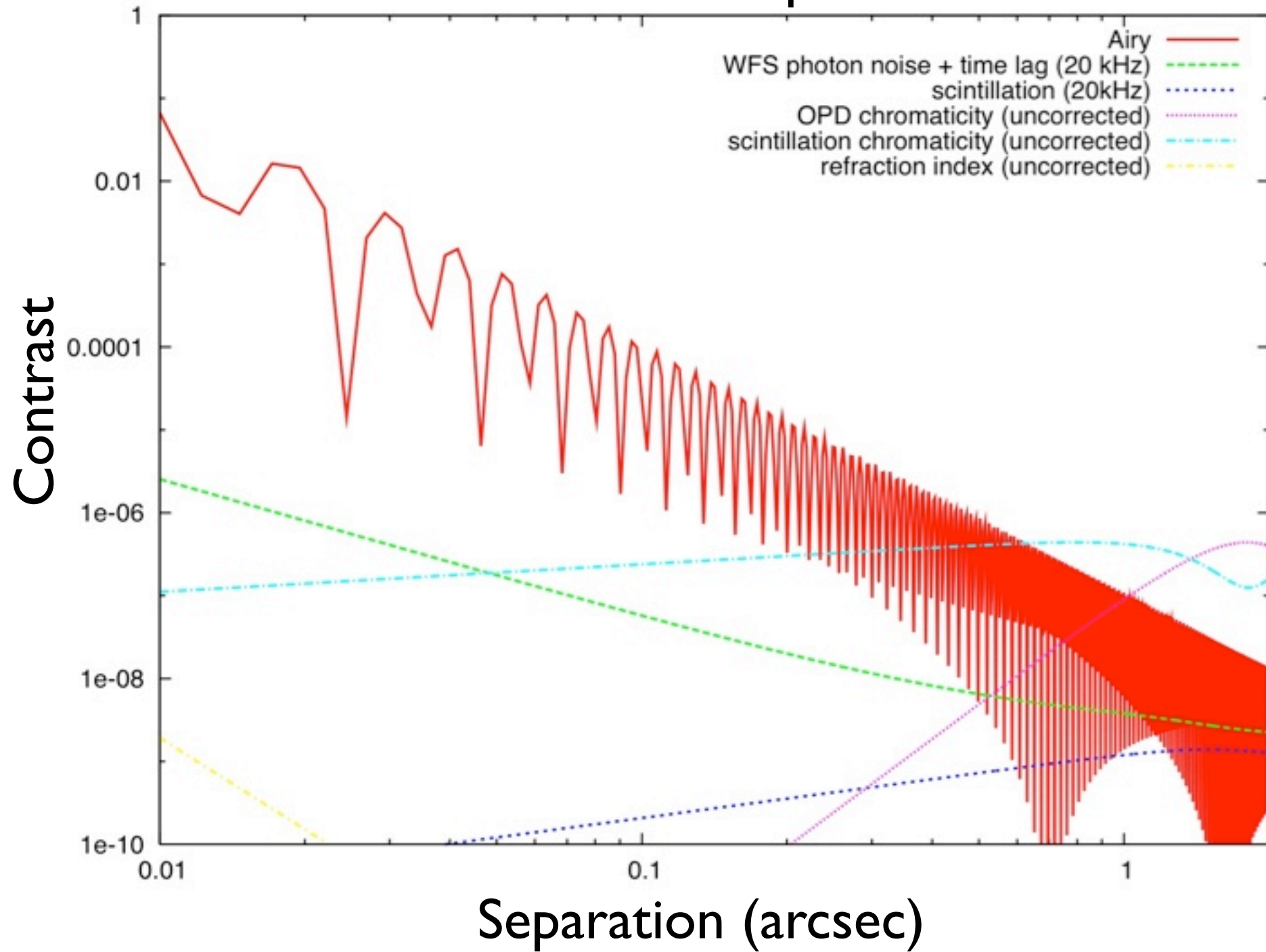
Speckle noise from Halo = $3e-6 \times 1/\sqrt{t(s)}$

in 1 hr, 3-sigma detection limit =

$1.5e-7$ (no differential detection)

$1e-8$ (differential detection, 1/4 photons)

30-m telescope



30m telescope, very good ExAO + slow near-IR correction

14x more photons in planet and star, contrast 14x better

still $\sim 1e4$ ph/s/speckle ($7e-7$ contrast)

Photon noise from Halo = $7e-9 \times 1/\sqrt{t(s)}$

Speckle noise from Halo = $2e-7 \times 1/\sqrt{t(s)}$

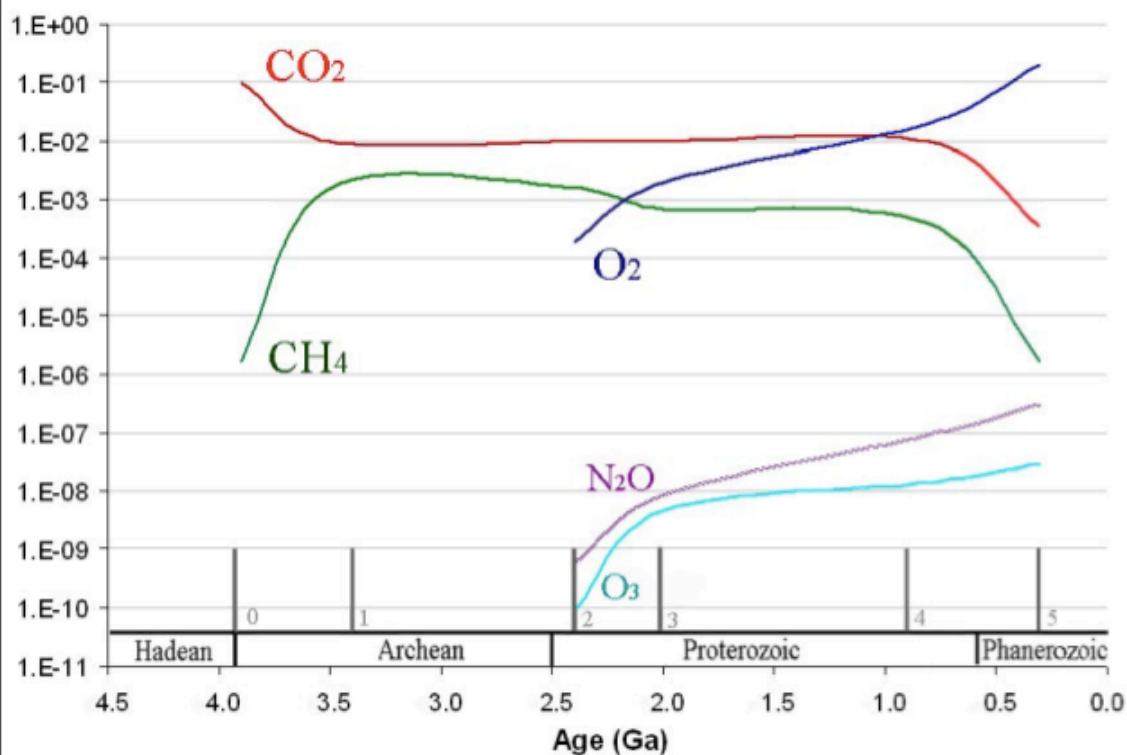
in 1hr, 3-sigma detection limit =

$1.1e-8$ (no differential detection)

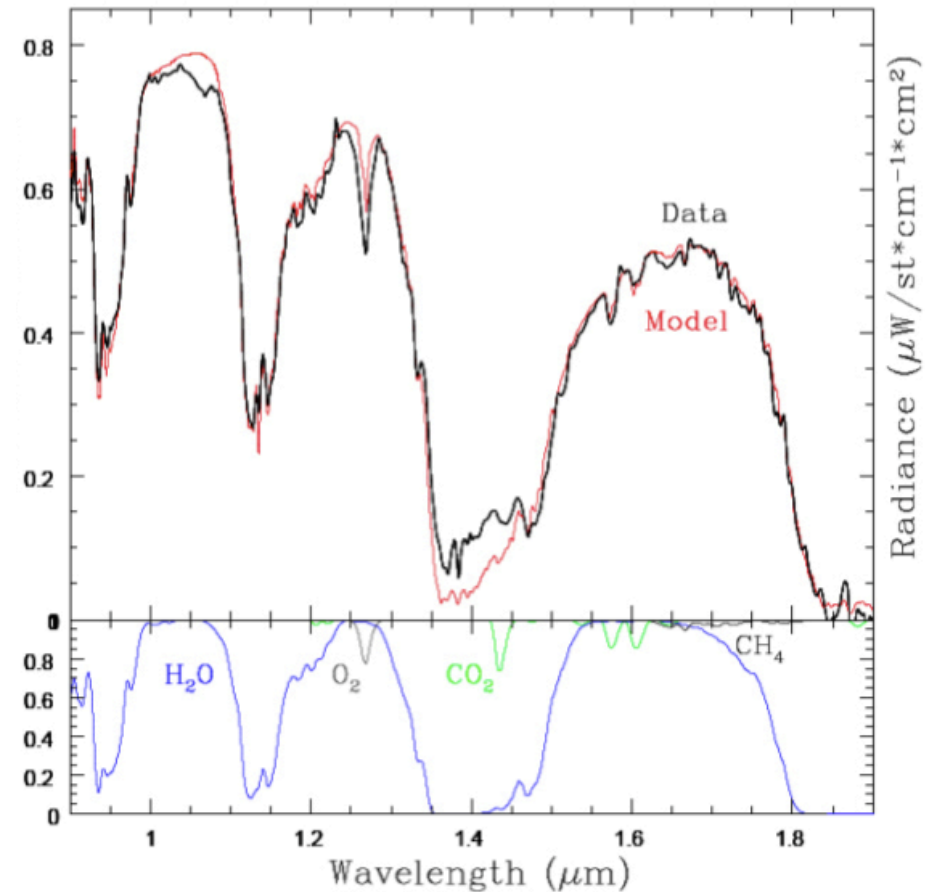
$7e-10$ (differential detection, assuming 1/4 photons)

Near-IR Earth spectra

- Water is easiest to detect
- CO₂, CH₄, O₂



Kasting 2004



Turnbull et al 2006