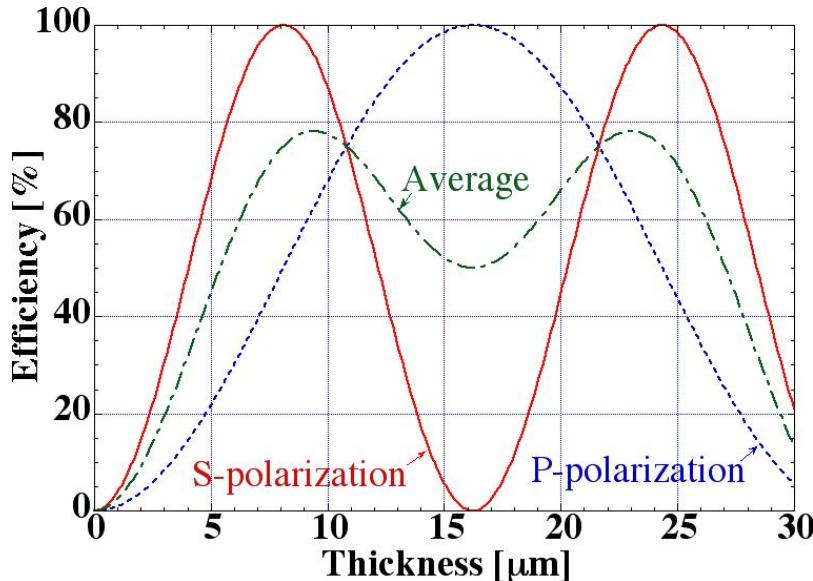


Birefringence Volume Grating

$$\eta_S = \sin^2 \left\{ \frac{\pi(n_{\max} - n_{\min})t}{\Lambda(n_{\max} + n_{\min}) \sin 2\theta} \right\}$$

$$\eta_P = \sin^2 \left\{ \frac{\pi(n_{\max} - n_{\min})t \cos 2\theta}{\Lambda(n_{\max} + n_{\min}) \sin 2\theta} \right\}$$



Polarized diffraction efficiencies versus grating thickness t of Dicson's VPH grating (Polarizer).

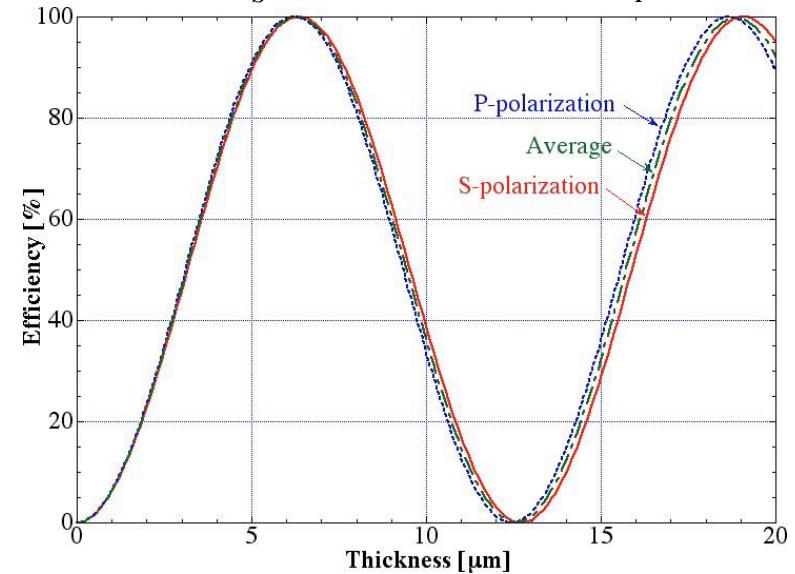
$$n_L = 1.46, n_H = 1.54, \theta_B = 48.5^\circ.$$

$$\frac{n_{S\max} - n_{S\min}}{(n_{S\max} + n_{S\min}) \sin 2\theta_S} = \frac{(n_{P\max} - n_{P\min}) \cos 2\theta_P}{(n_{P\max} + n_{P\min}) \sin 2\theta_P}$$

$$\frac{n_{S\max} - n_{S\min}}{(n_{S\max} + n_{S\min}) \cdot 2 \sin \theta_S \cos \theta_S} = \frac{(n_{P\max} - n_{P\min}) \cos 2\theta_P}{(n_{P\max} + n_{P\min}) \cdot 2 \sin \theta_P \cos \theta_P}$$

Snell's law

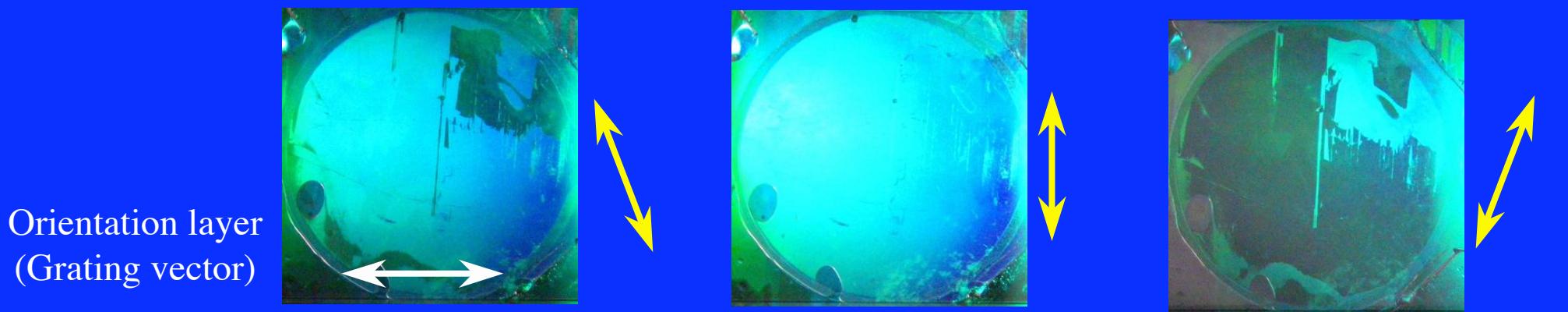
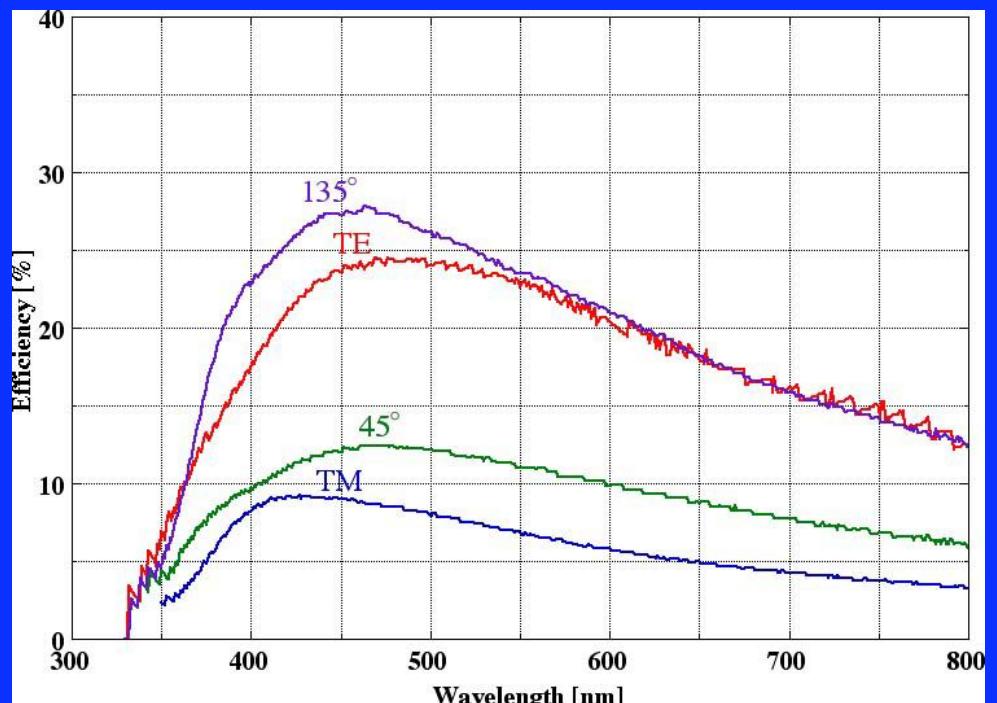
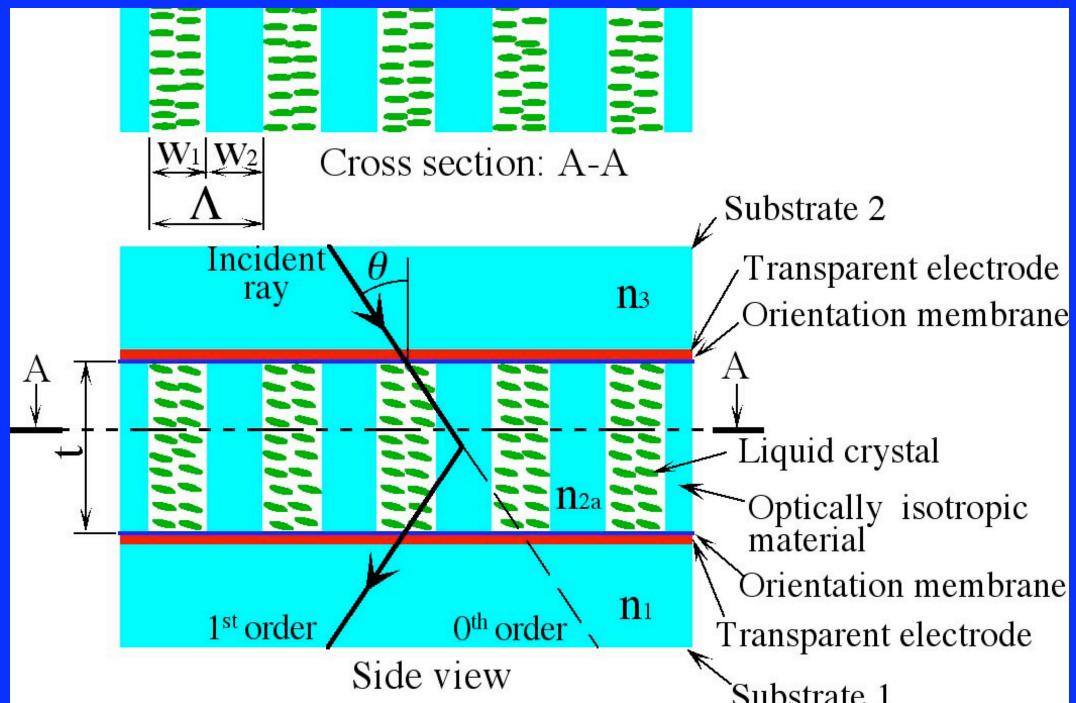
$$\frac{n_{S\max} - n_{S\min}}{\cos \theta_S} \approx \frac{(n_{P\max} - n_{P\min}) \cos 2\theta_P}{\cos \theta_P}$$



Polarized diffraction efficiencies versus grating thickness t of birefringence VPH grating.

$$n_L = 1.46, n_s = 1.544, n_p = 1.60, \theta_B = 45^\circ.$$

Birefringence Binary Bragg (3B) Grating



Polarizer angle: 60 ~ 70°

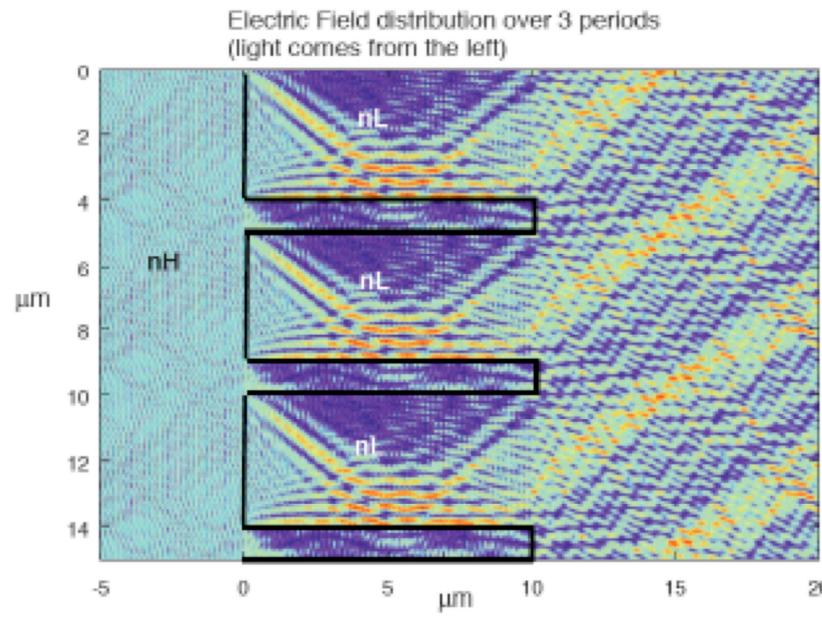
Polarizer angle: 90°

Polarizer angle: -60 ~ -70°

Images of the first order diffraction

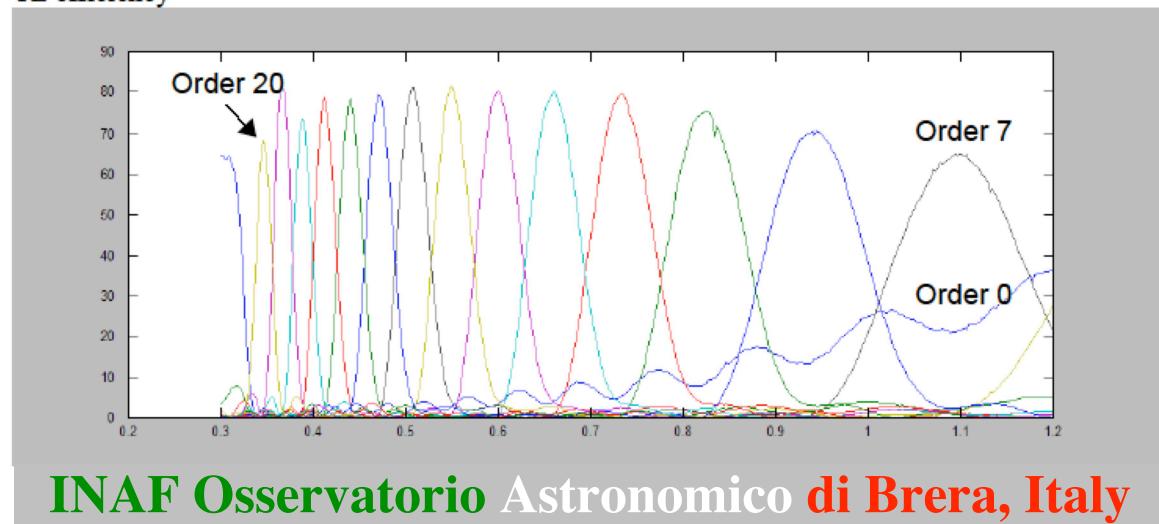
CITIZN Holdings Ltd.

Volume Binary Grating

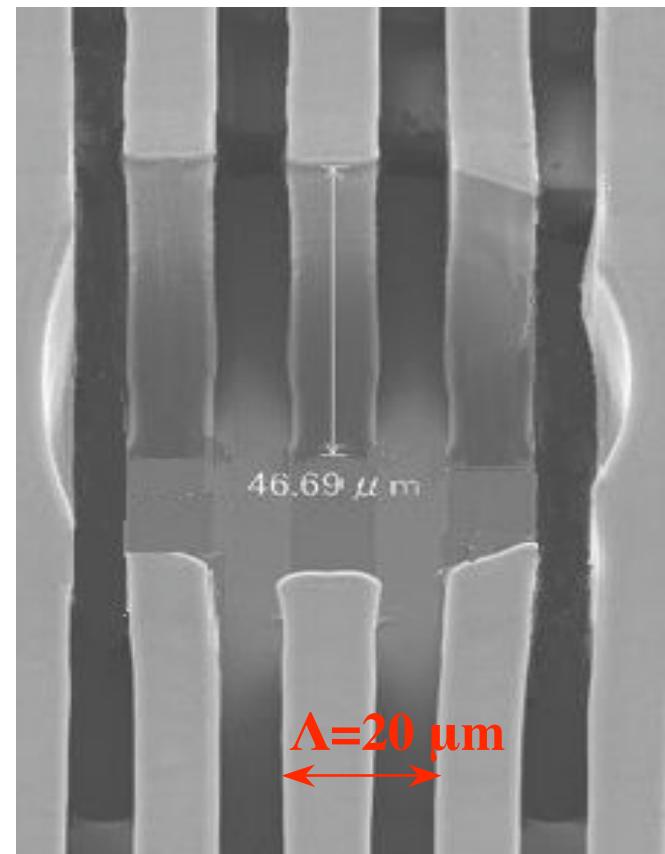


Configuration 1: ratio 9:1, $d = 11 \mu\text{m}$, $\Delta n = 0.19$

TE efficiency

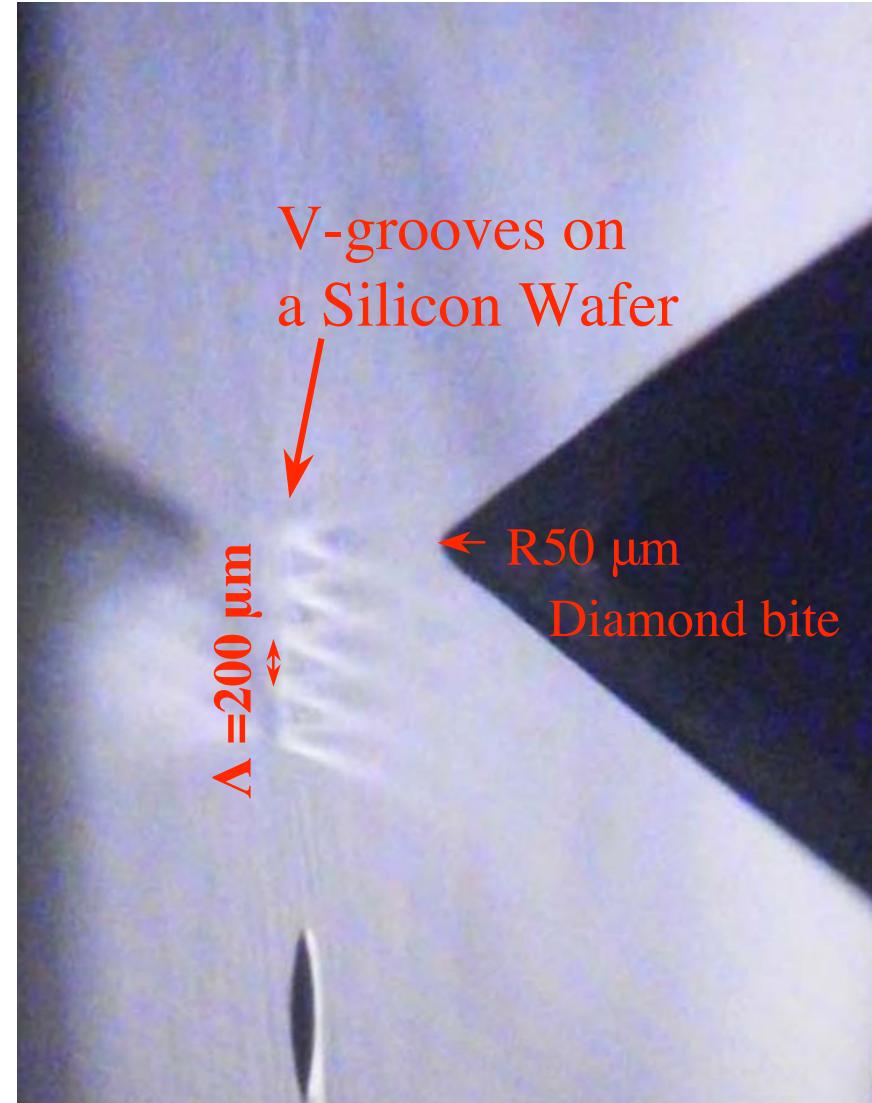
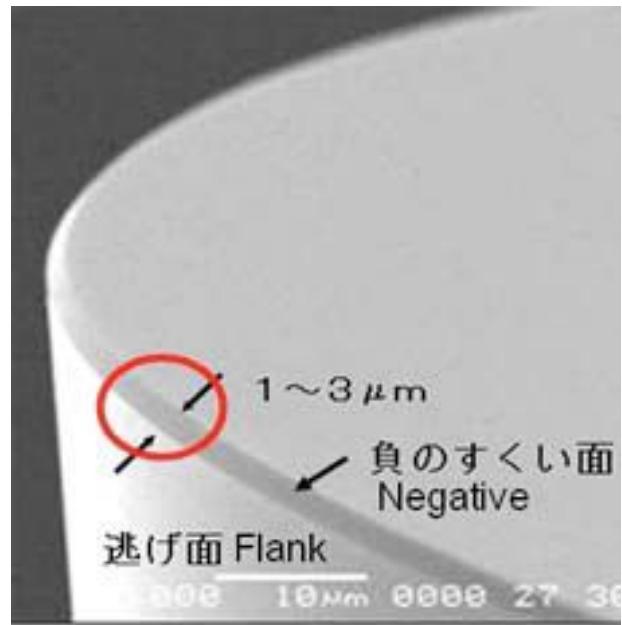
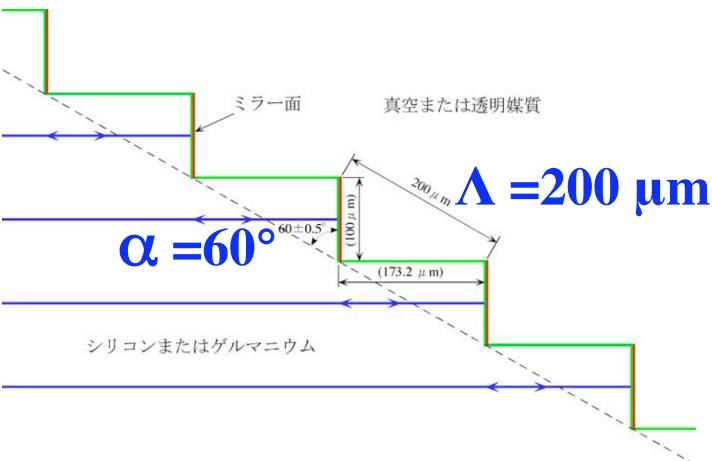


INAF Osservatorio Astronomico di Brera, Italy

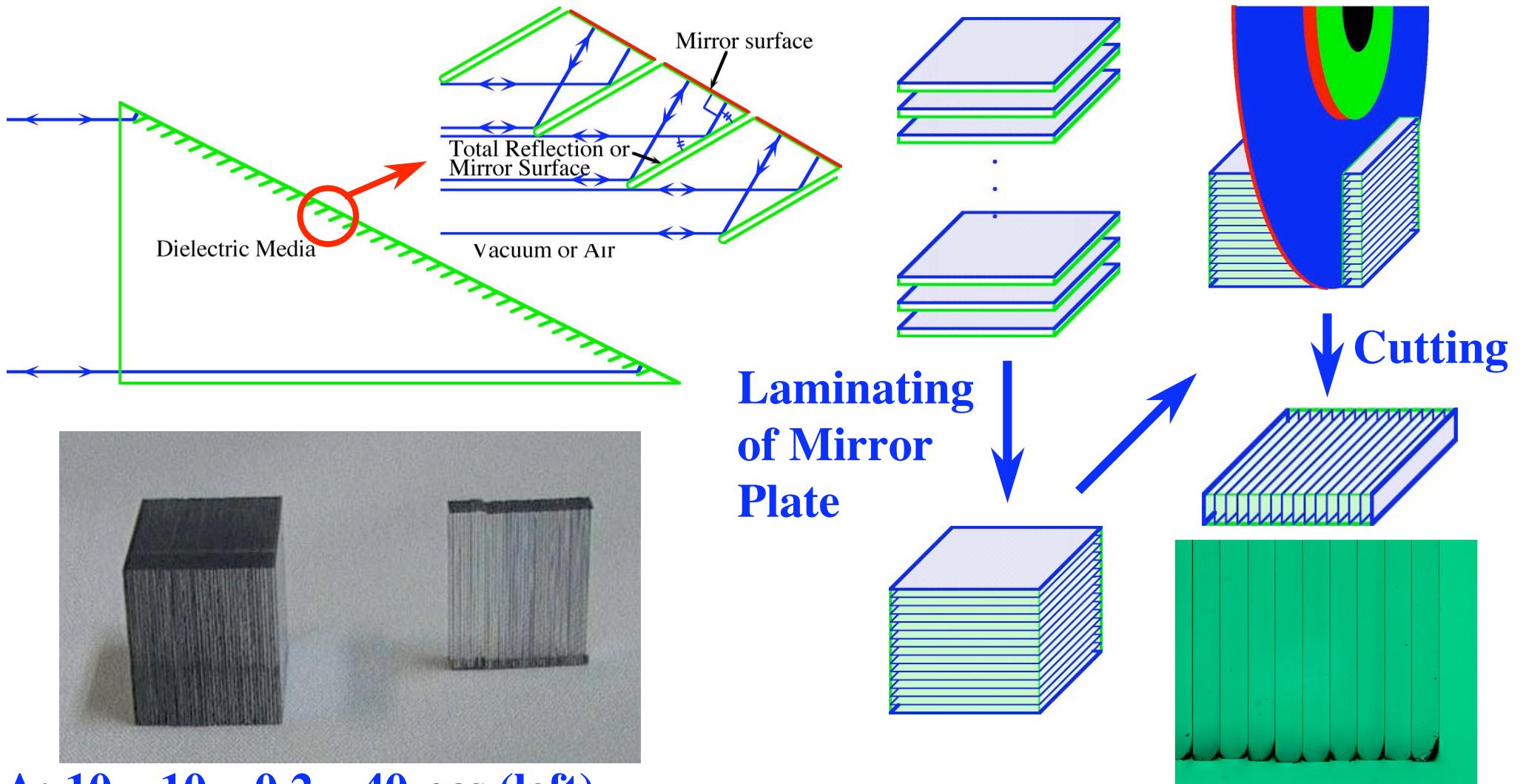


SEM image of grooves (L&S: 10 μm), tilting with 30°.
Photo resist: KMPR1000.
Nano-Technology Platform of Toyota Technological Institute

Si (Ge) Immersion Grating



Quasi-Bragg Immersion Grating



A: $10 \times 10 \times 0.2 \times 40$ pcs (left),
B: $1.5 \times 10 \times 0.2 \times 40$ pcs (right)
Fabricated by Kogaku-Giken Ltd.

2nd trial fabrication is performing
at NTT-AT Ltd.